

THORPE DESIGN, INC.
410 BEATRICE COURT SUITE A
BRENTWOOD, CA 94513

BLD18-4516.DFO1

PCI

OFFICE

HYDRAULIC CALCULATIONS

FOR

NEW RESIDENCE
49 DORCHESTER DRIVE
SANTA ROSA, CA
DESIGN/LAYOUT BY: ANGEL AMEZCUA
FILE NUMBER: 19-009
DATE: JAN 16, 2019

COUNTY OF SONOMA
FIRE & EMERGENCY SERVICE DEPT.
REVIEWED
FOR CODE COMPLIANCE

-DESIGN DATA-

OCCUPANCY CLASSIFICATION: RESIDENTIAL
GPM REQ. PER HEAD: 13 GPM
SPRINKLER SPACING: 16 X 16 SQ. FT.
NUMBER OF SPRINKLERS CALCULATED: 2 sprinklers
AUTHORITY HAVING JURISDICTION: SONOMA COUNTY
CONTRACTOR CERTIFICATION NUMBER: 541016

-SPRINKLERS-

MANUFACTURER: TYCO
MODEL: FLAT PLATE (TY3596)
SIZE: 1/2"
K-FACTOR: 4.9K
TEMP. RATING: 160 DEG.

-WATER FLOW-

STATIC: 67
RESIDUAL: 56
FLOW: 100 GPM
PROVIDED BY: CALIFORNIA AMERICAN WATER

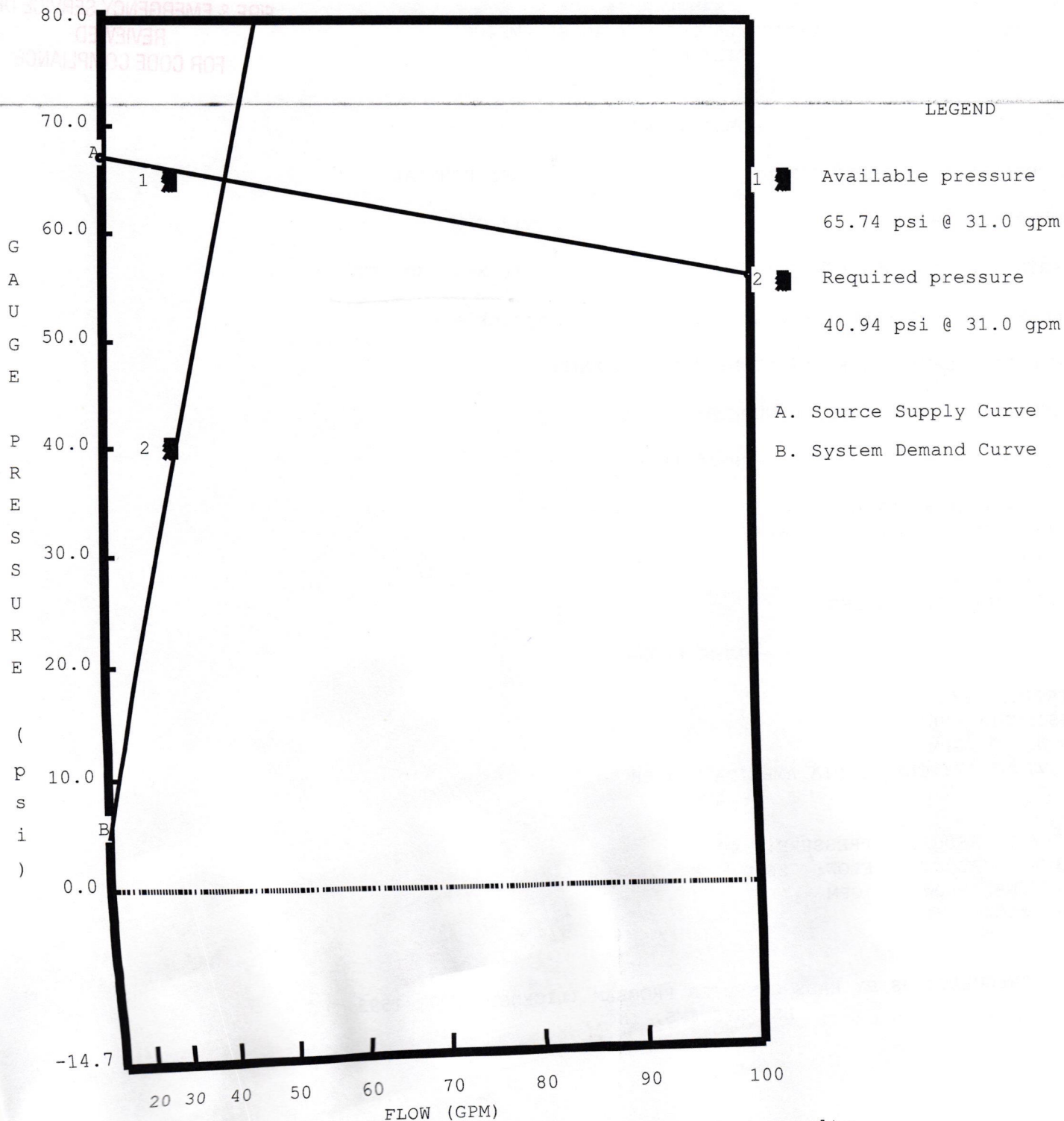
-DEMAND-

SPRINKLER REQUIRED PRESSURE: 40.9
SPRINKLER REQUIRED FLOW: 26.0
ADDITIONAL FLOWS: 5 GPM
TOTAL FLOW: 31.0

CALCULATIONS BY HASS COMPUTER PROGRAM (LICENSE # 27111593)
HRS SYSTEMS, INC..

WATER SUPPLY ANALYSIS

Static: 67.00 psi Resid: 56.00 psi Flow: 100.0 gpm



Note: (1) Dashed Lines indicate extrapolated values from Test Results

DATE: 1/16/2019 TER DRIVE (SONOMA COUNTY)\CALCS\19-009 49 DORCHESTER DR.SDF
 JOB TITLE:

NFPA WATER SUPPLY DATA

SOURCE NODE TAG	STATIC PRESS. (PSI)	RESID. PRESS. (PSI)	FLOW @ (GPM)	AVAIL. PRESS. (PSI)	TOTAL @ DEMAND (GPM)	REQ'D PRESS. (PSI)
SOURCE	67.0	56.0	100.0	65.7	31.0	40.9

Available pressure is 24.8 psi (38%) greater than required pressure.

AGGREGATE FLOW ANALYSIS:

TOTAL FLOW AT SOURCE	31.0 GPM
TOTAL HOSE STREAM ALLOWANCE AT SOURCE	0.0 GPM
OTHER HOSE STREAM ALLOWANCES	5.0 GPM
TOTAL DISCHARGE FROM ACTIVE SPRINKLERS	26.0 GPM

NODE ANALYSIS DATA

NODE TAG	ELEVATION (FT)	NODE TYPE	PRESSURE (PSI)	DISCHARGE (GPM)	NOTES
1	-1.5	- - - -	40.4	- - -	
2	-1.5	- - - -	36.4	- - -	
3	-1.5	- - - -	32.8	- - -	
4	2.5	HOSE STREAM	30.7	5.0	
5	3.5	- - - -	29.9	- - -	
F1	5.0	- - - -	29.1	- - -	
F2	5.0	- - - -	26.1	- - -	
6	6.5	- - - -	25.4	- - -	
7	10.0	- - - -	23.5	- - -	
8	9.5	- - - -	16.4	- - -	
9	9.5	- - - -	9.7	- - -	
9A	9.5	- - - -	9.7	- - -	
10	11.0	- - - -	8.1	- - -	
11	11.0	- - - -	8.1	- - -	
12	13.0	- - - -	17.4	- - -	
S1	9.0	- - - -	9.9	- - -	
S2	10.5	K= 4.90	7.0	13.0	
S3	10.5	K= 4.90	7.1	13.0	
SOURCE	0.0	SOURCE	40.9	31.0	

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 JOB TITLE:

NFPA PIPE DATA

Pipe Tag	K-fac	Add Fl	Fl To	Vel	Fit:	L	C	(Pt)	Notes	
Frm Node	El (ft)	PT	(q)	Node/	Eq.Ln.	F		(Pe)		
To Node	El (ft)	PT	Tot.(Q)	Disch	(ft.)	T	Pf/ft.	(Pf)		
				Act ID						
Pipe: SOURCE	Source	0.0		5.8		25.00	150	0.5		
SOURCE	0.0	40.9	31.0	2	K1.500	T: 8.0	8.00	-0.6		
1	-1.5	40.4	31.0		1.481	33.00	0.036	1.2		
<hr/>										
Pipe: 1			0.0	Fixed Pressure Loss Device						
1	-1.5	40.4	31.0	3		4.0 psi,	31.0 gpm			
2	-1.5	36.4	31.0							
Pipe: 2		0.0	0.0	5.0		125.00	150	3.6		
2	-1.5	36.4	31.0	4	S1.500	4E:16.0	16.00	0.0		
3	-1.5	32.8	31.0		1.593	141.00	0.025	3.6		
Pipe: 3		H.S.	5.0	Disch	5.6	4.00	150	2.1		
3	-1.5	32.8	26.0	5	L1.500	E: 4.0	7.00	1.7		
4	2.5	30.7	31.0		1.505	G: 3.0	11.00	0.033	0.4	
Pipe: 4		0.0	0.0	4.7		3.00	150	0.8		
4	2.5	30.7	26.0	F1	L1.500	2E: 8.0	11.00	0.4		
5	3.5	29.9	26.0		1.505	R: 3.0	14.00	0.024	0.3	
Pipe: 5		0.0	0.0	4.2		1.50	150	0.8		
5	3.5	29.9	26.0	F2	Y1.500	C: 7.0	7.00	0.6		
F1	5.0	29.1	26.0		1.598	8.50	0.018	0.2		
Pipe: F1			0.0	Fixed Pressure Loss Device						
F1	5.0	29.1	26.0	6		3.0 psi,	26.0 gpm			
F2	5.0	26.1	26.0							
Pipe: F2		0.0	0.0	4.2		1.50	150	0.7		
F2	5.0	26.1	26.0	7	Y1.500	2R: 2.0	2.00	0.6		
6	6.5	25.4	26.0		1.598	3.50	0.018	0.1		
Pipe: 6		0.0	14.3	12	4.2	15.58	150	2.0		
6	6.5	25.4	11.7	8	Y1.500	E: 9.0	10.00	1.5		
7	10.0	23.5	26.0		1.598	R: 1.0	25.58	0.018	0.5	
Pipe: 7		0.0	0.0	6.3		64.92	150	7.0		
7	10.0	23.5	11.7	9	Y0.750	3E:21.0	28.00	-0.2		
8	9.5	16.4	11.7		0.874	7R: 7.0	92.92	0.078	7.3	
Pipe: 8		0.0	0.0	6.3		33.75	150	6.7		
8	9.5	16.4	11.7	10	Y0.750	7E:49.0	52.00	0.0		
9	9.5	9.7	11.7		0.874	3R: 3.0	85.75	0.078	6.7	
Pipe: 9		0.0	13.0	S2	6.3	11.17	150	1.6		
9	9.5	9.7	-1.3	11	Y0.750	R: 1.0	1.00	0.6		
10	11.0	8.1	11.7		0.874	12.17	0.078	1.0		

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JOB TITLE:

Pipe Tag	K-fac	Add Fl	Fl To	Vel	Fit:	L	C	(Pt)	Notes
Frm Node	El (ft)	PT	(q)	Node/	Nom ID	Eq.Ln.	F	(Pe)	
To Node	El (ft)	PT	Tot.(Q)	Disch	Act ID	(ft.)	T	Pf/ft.	(Pf)
Pipe: 9A	0.0	0.0		0.0			1.67	150	0.0
9A	9.5	9.7	0.0		Y0.750	R: 1.0	1.00		0.0
9	9.5	9.7	0.0		0.874		2.67	0.000	0.0
Pipe: 10	0.0	13.0	S2	0.7			15.75	150	0.0
11	11.0	8.1	-11.7	9	Y0.750	R: 1.0	1.00		0.0
10	11.0	8.1	1.3		0.874		16.75	0.001	0.0
Pipe: 11	0.0	13.0	S3	7.6	5E:35.0		46.08	150	9.2
12	13.0	17.4	1.3	10	Y0.750	2T: 6.0	44.00		-0.9
11	11.0	8.1	14.3		0.874	3R: 3.0	90.08	0.112	10.1
Pipe: 12	0.0	0.0		7.6	2E:14.0		23.67	150	6.1
7	10.0	23.5	14.3	11	Y0.750	T: 3.0	19.00		1.3
12	13.0	17.4	14.3		0.874	2R: 2.0	42.67	0.112	4.8
Pipe: S1	0.0	0.0		0.0			6.92	150	0.2
S1	9.0	9.9	0.0		Y0.750	T: 3.0	3.00		0.2
9A	9.5	9.7	0.0		0.874		9.92	0.000	0.0
Pipe: S2	4.90	13.0	Disch	7.0			3.50	150	1.1
10	11.0	8.1	0.0		Y0.750	E: 7.0	10.00		-0.2
S2	10.5	7.0	13.0		0.874	T: 3.0	13.50	0.094	1.3
Pipe: S3	4.90	13.0	Disch	7.0			3.50	150	1.1
11	11.0	8.1	0.0		Y0.750	E: 7.0	10.00		-0.2
S3	10.5	7.1	13.0		0.874	T: 3.0	13.50	0.095	1.3

NOTES (HASS):

- (1) Calculations were performed by the HASS 8.8 computer program in accordance with NFPA13 (2016) under license no. 27111593 granted by HRS Systems, Inc. 208 Southside Square Petersburg, TN 37144 (931) 659-9760
- (2) The system has been calculated to provide an average imbalance at each node of 0.003 gpm and a maximum imbalance at any node of 0.054 gpm.
- (3) Total pressure at each node is used in balancing the system. Maximum water velocity is 7.6 ft/sec at pipe 11.
- (4) Items listed in bold print on the cover sheet are automatically transferred from the calculation report.
- (5) Available pressure at source node SOURCE under full flow conditions is

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64.89 psi with a flow of 40.95 gpm.

(6) PIPE FITTINGS TABLE

User Pipe Table Name: SIGMA1.PIP

PAGE: K MATERIAL: Copper HWC: 150

Diameter (in)	Equivalent Fitting Lengths in Feet									
	F	E	T	B	G	C	R	A	Q	
1.481	2.00	4.00	8.00	2.00	3.00	6.00	3.00	7.00	9.00	

PAGE: L MATERIAL: Copper HWC: 150

Diameter (in)	Equivalent Fitting Lengths in Feet							
	F	E	T	B	G	C	R	
1.505	2.00	4.00	8.00	2.00	3.00	6.00	3.00	

PAGE: S MATERIAL: PVC - Sch 40 HWC: 150

Diameter (in)	Equivalent Fitting Lengths in Feet								
	F	E	T	B	G	C	R	Z	
1.593	2.10	4.00	8.00	0.00	1.00	8.91	2.70	0.00	

PAGE: Y MATERIAL: Blazem HWC: 150

Diameter (in)	Equivalent Fitting Lengths in Feet									
	F	E	T	B	G	C	R	Z		
0.874	1.00	7.00	3.00	0.00	1.00	7.00	1.00	10.00		
1.598	2.00	9.00	8.00	1.00	1.00	7.00	1.00	10.00		

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CALIFORNIA
AMERICAN WATER

BLD18-4516.DF01
PCI

August 8, 2018

**SUBJECT: HYDRANT FLOW TEST – LARKFIELD SYSTEM
DARBSTER PLACE**

To whom it may concern:

On June 15, 2018 at approximately 1:45 P.M., a flow test was conducted by California American Water staff using fire hydrants located along Folsom Blvd. (see Attachment “A”- Location Map). These fire hydrants are located in the Suburban System of California American Water Sacramento District. The following measurements were collected during the flow test:

Residual Hydrant (FH # 3105)

Static Pressure = 72 psi

Residual Pressure = 62 psi

Flowing Hydrant (FH # 3101)

Outlet Diameter = 2.4 inches

Pitot Pressure = 21 psi

The calculated results of this flow test indicate that, based on the data collected at the time and date tested and under the exhibited system operational conditions, the distribution system in this area would be capable of delivering a flow of approximately **1,688 gpm, for a 2 hour duration, with a 20 psi residual system pressure** (see fire hydrant flow test information, Attachment “B”).

Hydrant flow tests are known to fluctuate with operational conditions, routine maintenance, and system demands, which are influenced by time of day, season, temperature, and day of the week. Static water pressures fluctuate in accordance with system demands; water systems are designed with the intent of meeting CPUC GO 103 & Title 22 requirements, with minimum operating pressures of 40 psi for normal operation, 30 psi for peak hour and 20 psi for fire flow conditions.

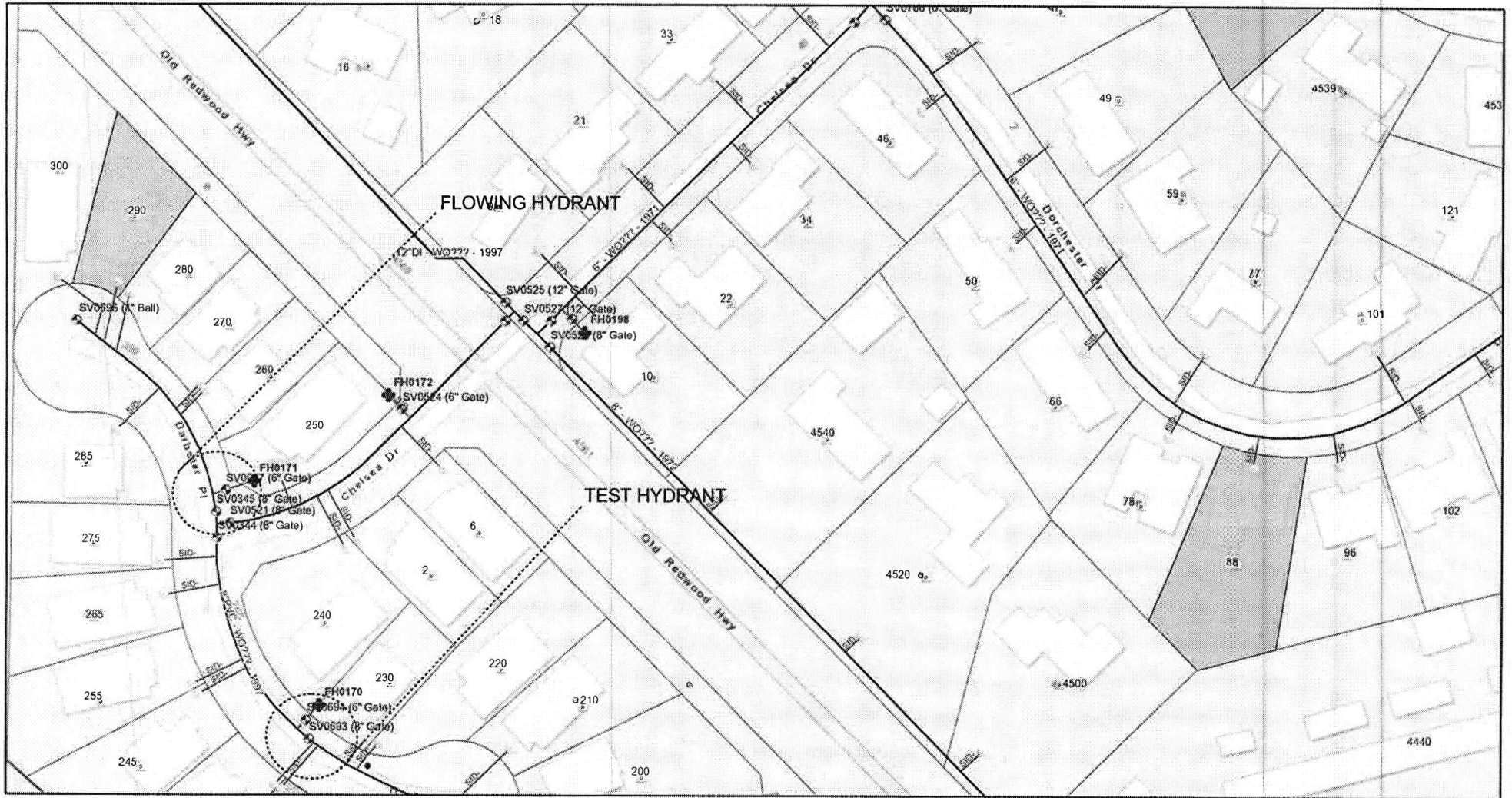
I hope this information satisfies your needs. Please contact me at (916) 568-4210, or at spencer.phillips@amwater.com if you have questions or require additional information.

Sincerely,

Spencer Phillips
California American Water

2 Attachments

Attachment "A"

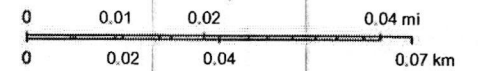


May 29, 2018

CALIFORNIA AMERICAN WATER; LARKFIELD DISTRICT - FIRE HYDRANT FLOW TEST LOCATION MAP

1:1,128

- Water - Meter Pit
- Water - Lateral Service
- ServiceAreaBoundary
- Property - Assessment
- Water - Lateral Fire Service
- Domestic
- Premise
- As-Built
- Hydrant Laterals
- Hydrant Laterals
- LK_NewMeters
- MapCall_OperatingCenter_Index
- Override 1
- Property - Property Point



Sources: Esri, HERE, Garmin, USGS, Intermap, INCREMENT P, NRCan, Esri Japan, METI, Esri China (Hong Kong), Esri Korea, Esri (Thailand), NGCC, © OpenStreetMap contributors, and the GIS User Community



**CALIFORNIA
AMERICAN WATER**

FIRE HYDRANT FLOW TEST INFORMATION

Project Address: Darbster Place
CAW System: Larkfield
Test Date & Time: 6/15/2018; 1:45 P.M.
Performed By: Jason C., Corey K.

Residual Hydrant No.: FH-170 **Location:** Along Darbster Pl.
Flowing Hydrant No.: FH-171 (see Location Map in Attachment "A")

Field Observations:

Static Pressure	71	psi	Pressure measured at the residual hydrant with no hydrants flowing
Residual Pressure	52	psi	Pressure measured at the residual hydrant when flow hydrant is flowing
Pitot Pressure, <i>P</i>	41	psi	Pitot gage reading taken from the outlet of flowing hydrant
Outlet Diameter, <i>d</i>	2.4	in	Opening size of hydrant outlet being flowed

Calculations:

a. Determination of Discharge

$$Q_F = 29.83 c d^2 \sqrt{P}$$

Where:

c = coefficient of discharge, 0.9

d = diameter of outlet, in

P = pitot gauge pressure, psi

$Q_F =$ 990 gpm Actual hydrant flow during test

b. Determining Available Flow

$$Q_R = Q_F \times \frac{h_r^{0.54}}{h_f^{0.54}}$$

Where:

h_r = pressure difference between static pressure and the desired residual pressure of 20 psi

h_f = pressure difference between static pressure and the residual pressure, psi

$Q_R =$ 1,688 gpm Available flow @ 20 psi residual pressure

The calculated results shown above indicate that the distribution system in this area where the hydrant was tested exhibited that it would be capable of delivering a flow of approximately 1,688 gpm at 20 psi residual pressure.

Notes: The above flow test and calculations were in accordance with the recommended practices for fire flow testing per AWWA M17 Manual and NFPS 291 Standards. The company provides no warranty that it will supply at any specific flows, quantities or pressures for fire protection or other purposes, except as required by law. For questions, please contact Spencer Phillips at (916) 568-4210 or at

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