



T R U N O R T H

707 Hahman Drive #2619

Santa Rosa, CA 95405

707.308.8638

www.TruNorth.co

STRUCTURAL CALCULATIONS PACKAGE

FOR:

LANDS OF WINGS CAPITAL LLC

ARVIN BABU
2199 DIAMOND MOUNTAIN RD.
CALISTOGA, CALIFORNIA 94515
APN: 120-240-015

DESIGN PROFESSIONAL

TRUNORTH
DANIEL BYRNE, RCE 80078
DAN@TRUNORTH.CO





TABLE OF CONTENTS:

LOAD DETERMINATIONS

LATERAL ANALYSIS

BEAM CALCULATIONS

FOUNDATION CALCULATIONS

Limitations:

The calculations and recommendations provided within this package are limited to structural elements directly affected as a result of the proposed improvements. Any deviations from the approved plans or changes to the proposed scope of work or design, including but not limited to modifications to the size, location, or nature of the improvements, shall be immediately communicated in writing to the design professional prior to construction with the understanding that additional structural analysis and design may be required. Any unexpected conditions encountered during construction should be immediately communicated to the Design Professional.



T R U N O R T H

LATERAL ANALYSIS

ASCE 7-16 Seismic Base Shear

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Seismic Base Shear Analysis

Specific Description: Seismic Base Shear for New Deck

Risk Category

Calculations per ASCE 7-16

Risk Category of Building or Other Structure : "II" : All Buildings and other structures except those listed as Category I, III, and IV [SCE 7-16, Page 4, Table 1.5-1](#)

Seismic Importance Factor = 1 [ASCE 7-16, Page 5, Table 1.5-2](#)

USER DEFINED Ground Motion

[ASCE 7-16 11.4.2](#)

Max. Ground Motions, 5% Damping

$S_S = 1.906$ g, 0.2 sec response

$S_1 = 0.7120$ g, 1.0 sec response

For the closest datapoint grid location . . .

Latitude = 0.000 deg North

Longitude = 0.000 deg West

Site Class, Site Coeff. and Design Category

Classification: "C" : Shear Wave Velocity 1,200 to 2,500 ft/sec = **C** [ASCE 7-16 Table 20.3-1](#)

Site Coefficients F_a & F_v $F_a = 1.20$ [ASCE 7-16 Table 11.4-1 & 11.4-2](#)

(using straight-line interpolation from table values)

$F_v = 1.40$

Maximum Considered Earthquake Acceleration $S_{MS} = F_a * S_s = 2.287$ [ASCE 7-16 Eq. 11.4-1](#)

$S_{M1} = F_v * S_1 = 0.997$ [ASCE 7-16 Eq. 11.4-2](#)

Design Spectral Acceleration $S_{DS} = S_{MS} * 2/3 = 1.525$ [ASCE 7-16 Eq. 11.4-3](#)

$S_{D1} = S_{M1} * 2/3 = 0.665$ [ASCE 7-16 Eq. 11.4-4](#)

Seismic Design Category = **D** [ASCE 7-16 Table 11.6-1 & -2](#)

Resisting System

[ASCE 7-16 Table 12.2-1](#)

Basic Seismic Force Resisting System . . .

Building Frame Systems

3.Steel ordinary concentrically braced frames

Response Modification Coefficient "R" = 3.25 [Building height Limits :](#)

System Overstrength Factor "Wo" = 2.00 Category "A & B" Limit: No Limit

Deflection Amplification Factor "Cd" = 3.25 Category "C" Limit: No Limit

Category "D" Limit: Limit = 35j

Category "E" Limit: Limit = 35j

Category "F" Limit: Limit = 35j

NOTE! See ASCE 7-16 for all applicable footnotes

Lateral Force Procedure

[ASCE 7-16 Section 12.8.2](#)

Equivalent Lateral Force Procedure

[The "Equivalent Lateral Force Procedure" is being used according to the provisions of ASCE 7-16 12.8](#)

Determine Building Period

[Use ASCE 12.8-7](#)

Structure Type for Building Period Calculation: STEEL 100% Moment Resisting Frame

"Ct" value = 0.028 "hn" : Height from base to highest level = 20.0 ft

"x" value = 0.80

"Ta" Approximate fundamental period using Eq. 12.8-7 : $T_a = C_t * (h_n^x) = 0.308$ sec

"TL" : Long-period transition period per ASCE 7-16 Maps 22-14 -> 22-17 = 8.000 sec

Building Period "Ta" Calculated from Approximate Method set = 0.308

"Cs" Response Coefficient

[ASCE 7-16 Section 12.8.1.1](#)

S_{DS} : Short Period Design Spectral Response = 1.525 From Eq. 12.8-2, Preliminary $C_s = 0.469$

"R" : Response Modification Factor = 3.25 From Eq. 12.8-3 & 12.8-4, C_s need not exceed = 0.665

"I" : Seismic Importance Factor = 1 From Eq. 12.8-5 & 12.8-6, C_s not be less than = 0.110

Cs : Seismic Response Coefficient = 0.4692

Project Title: Lands of Wings Capital LLC
 Engineer: Daniel Byrne
 Project ID:
 Project Descr: New Deck

ASCE 7-16 Seismic Base Shear

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

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(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Seismic Base Shear Analysis

Seismic Base Shear

ASCE 7-16 Section 12.8.1

$C_s = 0.4692$ from 12.8.1.1

W (see Sum W_i below) = 9.32 k

Seismic Base Shear $V = C_s * W = 4.37$ k

Vertical Distribution of Seismic Forces

ASCE 7-16 Section 12.8.3

"k" : hx exponent based on $T_a = 1.00$

Table of building Weights by Floor Level...

Level #	W_i : Weight	H_i : Height	$(W_i * H_i^k)$	C_{vx}	$F_x = C_{vx} * V$	Sum Story Shear	Sum Story Moment
1	9.32	8.00	74.58	1.0000	4.37	4.37	0.00
Sum $W_i =$	9.32 k	Sum $W_i * H_i =$	74.58 k-ft		Total Base Shear =	4.37 k	Base Moment = 35.0 k-ft

Diaphragm Forces : Seismic Design Category "B" to "F"

ASCE 7-16 12.10.1.1

Level #	W_i	F_i	Sum F_i	Sum W_i	F_{px} : Calcd	F_{px} : Min	F_{px} : Max	F_{px}	Dsgn. Force
1	9.32	4.37	4.37	9.32	4.37	2.84	5.69	4.37	4.37

W_{px} Weight at level of diaphragm and other structure elements attached to it.

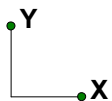
F_i Design Lateral Force applied at the level.

Sum F_i Sum of "Lat. Force" of current level plus all levels above

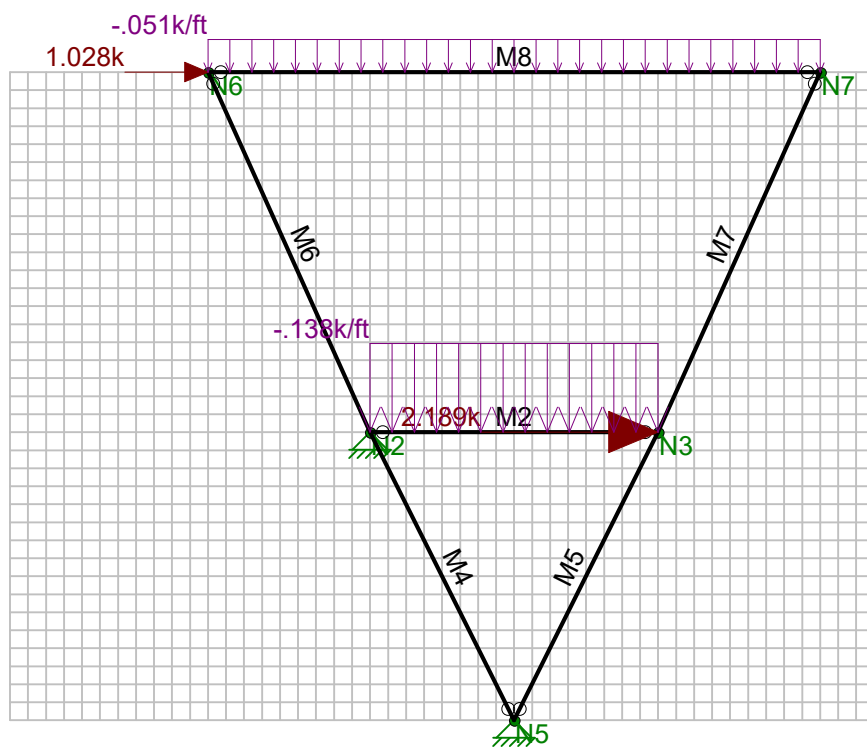
MIN Req'd Force @ Level ... $0.20 * S_{DS} * I * W_{px}$

MAX Req'd Force @ Level ... $0.40 * S_{DS} * I * W_{px}$

F_{px} : Design Force @ Level ... $W_{px} * \text{SUM}(x \rightarrow n) F_i / \text{SUM}(x \rightarrow n) w_i$, x = Current level, n = Top Level



STEEL FRAME ANALYSIS IN LONGITUDINAL DIRECTION



September 23, 2024

3:18 PM

Deck RISA Model.r2e

**Global**

Display Sections for Member Calcs 5

Joint Coordinates

Joint Label	X Coordinate (ft)	Y Coordinate (ft)
N2	10	8
N3	18	8
N5	14	0
N6	5.5	18
N7	22.5	18

Boundary Conditions

Joint Label	X Translation (k/in)	Y Translation (k/in)	Rotation (k-ft/rad)
N5	Reaction	Reaction	
N2	Reaction	Reaction	

Member Data

Member Label	I Joint	J Joint	Area in ²	Moment of Inertia in ⁴	Elastic Modulus ksi	End Releases I-End	J-End	Length ft
M2	N2	N3	5.24	42.5	29000	PIN	PIN	8
M4	N5	N2	5.24	28.6	29000	PIN		8.944
M5	N5	N3	5.24	28.6	29000	PIN		8.944
M6	N2	N6	5.24	28.6	29000		PIN	10.966
M7	N3	N7	5.24	28.6	29000		PIN	10.966
M8	N6	N7	5.24	42.5	29000	PIN	PIN	17

Joint Loads/Enforced Displacements

Joint Label	[L]oad or [D]isplacement	Direction	Magnitude (k, k-ft, in, rad)
N6	L	X	1.028
N3	L	X	2.189

Member Distributed Loads

Member Label	Direction	Start Magnitude (k/ft, F)	End Magnitude (k/ft, F)	Start Location (ft or %)	End Location (ft or %)
M2	Y	-.138	-.138	0	10
M8	Y	-.051	-.051	0	17

Joint Displacements

Joint Label	X Translation (in)	Y Translation (in)	Rotation (radians)
N2	0	0	-2.672e-3
N3	.002	-.002	-2.678e-3
N5	0	0	0
N6	.714	.321	0
N7	.713	-.323	0

Reactions

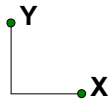
Joint Label	X Force (k)	Y Force (k)	Moment (k-ft)
N5	1.649	1.244	0

**Reactions**

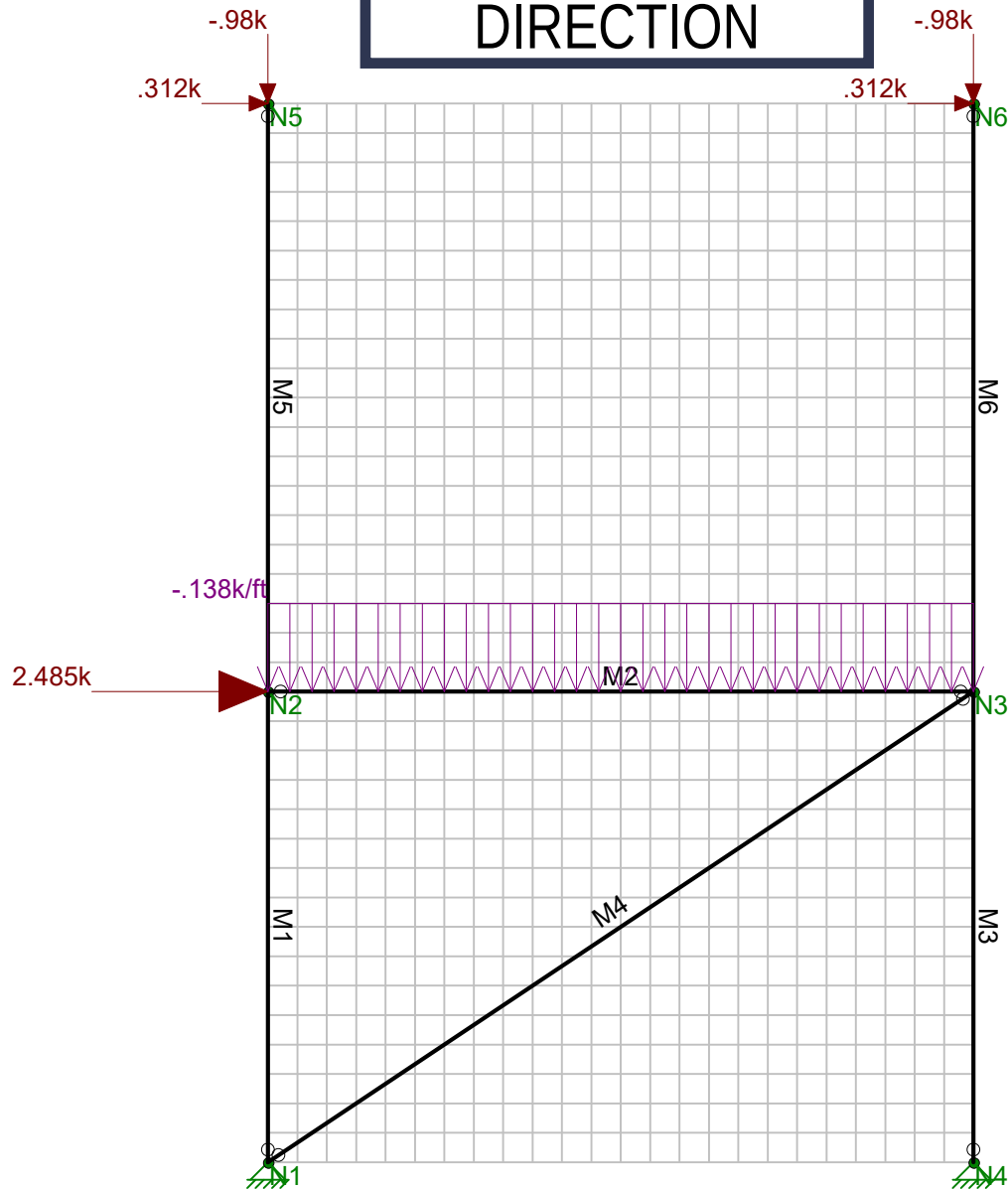
Joint Label	X Force (k)	Y Force (k)	Moment (k-ft)
N2	-4.866	.727	0
Totals:	-3.217	1.971	

Member Section Forces

Member Label	Section	Axial (k)	Shear (k)	Moment (k-ft)
M2	1	-3.638	.552	0
	2	-3.638	.276	.828
	3	-3.638	0	1.104
	4	-3.638	-.276	.828
	5	-3.638	-.552	0
M4	1	0	-.577	0
	2	0	-.577	-1.29
	3	0	-.577	-2.58
	4	0	-.577	-3.871
	5	0	-.577	-5.161
M5	1	1.388	-.572	0
	2	1.388	-.572	-1.28
	3	1.388	-.572	-2.56
	4	1.388	-.572	-3.839
	5	1.388	-.572	-5.119
M6	1	.687	.471	-5.161
	2	.687	.471	-3.871
	3	.687	.471	-2.58
	4	.687	.471	-1.29
	5	.687	.471	0
M7	1	.265	.467	-5.119
	2	.265	.467	-3.839
	3	.265	.467	-2.56
	4	.265	.467	-1.28
	5	.265	.467	0
M8	1	.317	.434	0
	2	.317	.217	1.382
	3	.317	0	1.842
	4	.317	-.217	1.382
	5	.317	-.433	0



STEEL FRAME ANALYSIS IN TRANSVERSE DIRECTION



September 24, 2024

10:46 AM

Deck Alt Direction RISA Model.r2e

Global

Display Sections for Member Calcs

5



T R U N O R T H

Joint Coordinates

Joint Label	X Coordinate (ft)	Y Coordinate (ft)
N1	0	0
N2	0	8
N3	12	8
N4	12	0
N5	0	18
N6	12	18

Boundary Conditions

Joint Label	X Translation (k/in)	Y Translation (k/in)	Rotation (k-ft/rad)
N1	Reaction	Reaction	
N4	Reaction	Reaction	
N5			
N6			

Member Data

Member Label	I Joint	J Joint	Area in ²	Moment of Inertia in ⁴	Elastic Modulus ksi	End Releases I-End J-End	Length ft
M1	N1	N2	5.24	28.6	29000	PIN	8
M2	N2	N3	5.24	42.5	29000	PIN PIN	12
M3	N4	N3	5.24	28.6	29000	PIN	8
M4	N1	N3	1.43	1.19	29000	PIN PIN	14.422
M5	N2	N5	5.24	28.6	29000	PIN	10
M6	N3	N6	5.24	28.6	29000	PIN	10

Joint Loads/Enforced Displacements

Joint Label	[L]oad or [D]isplacement	Direction	Magnitude (k, k-ft, in, rad)
N2	L	X	2.485
N5	L	X	.312
N6	L	X	.312
N5	L	Y	-.98
N6	L	Y	-.98

Member Distributed Loads

Member Label	Direction	Start Magnitude (k/ft, F)	End Magnitude (k/ft, F)	Start Location (ft or %)	End Location (ft or %)
M2	Y	-.138	-.138	0	12

Joint Displacements

Joint Label	X Translation (in)	Y Translation (in)	Rotation (radians)
N1	0	0	0
N2	.028	-.001	-1.739e-3
N3	.025	-.003	-1.708e-3
N4	0	0	0
N5	.454	-.002	0
N6	.447	-.004	0

Reactions

Joint Label	X Force (k)	Y Force (k)	Moment (k-ft)
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**Reactions**

Joint Label	X Force (k)	Y Force (k)	Moment (k-ft)
N1	-3.499	-.785	0
N4	.39	4.401	0
Totals:	-3.109	3.616	

Member Section Forces

Member Label	Section	Axial (k)	Shear (k)	Moment (k-ft)
M1	1	1.808	-.39	0
	2	1.808	-.39	-.78
	3	1.808	-.39	-1.56
	4	1.808	-.39	-2.34
	5	1.808	-.39	-3.12
M2	1	3.187	.828	0
	2	3.187	.414	1.863
	3	3.187	0	2.484
	4	3.187	-.414	1.863
	5	3.187	-.828	0
M3	1	4.401	-.39	0
	2	4.401	-.39	-.78
	3	4.401	-.39	-1.56
	4	4.401	-.39	-2.34
	5	4.401	-.39	-3.12
M4	1	-4.674	0	0
	2	-4.674	0	0
	3	-4.674	0	0
	4	-4.674	0	0
	5	-4.674	0	0
M5	1	.98	.312	-3.12
	2	.98	.312	-2.34
	3	.98	.312	-1.56
	4	.98	.312	-.78
	5	.98	.312	0
M6	1	.98	.312	-3.12
	2	.98	.312	-2.34
	3	.98	.312	-1.56
	4	.98	.312	-.78
	5	.98	.312	0



T R U N O R T H

BEAM CALCULATIONS

Wood Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Roof Rafters

CODE REFERENCES

Calculations per NDS 2018, IBC 2021, SDPWS 2021

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design

Load Combination IBC 2021

Wood Species : Western Cedars

Wood Grade : No.2

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

Fb + 700 psi

Fb - 700 psi

Fc - Prll 650 psi

Fc - Perp 425 psi

Fv 155 psi

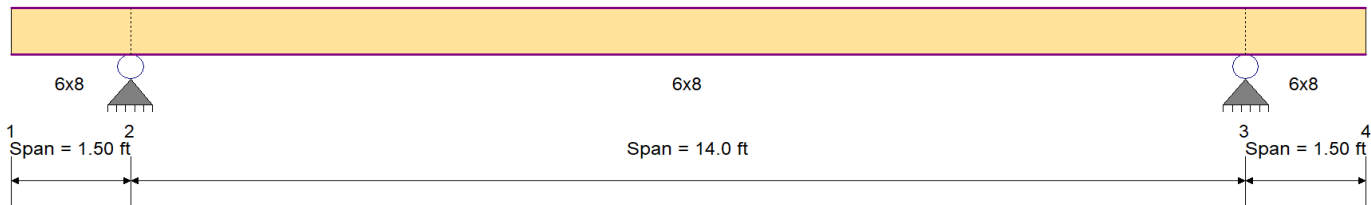
Ft 425 psi

E : Modulus of Elasticity

Ebend- xx 1000ksi

Eminbend - xx 370ksi

Density 22.47pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio				Maximum Shear Stress Ratio			
Section used for this span	=	0.056	1	Section used for this span	=	0.011	1
		6x8				6x8	
fb: Actual	=	35.01 psi		fv: Actual	=	1.50 psi	
F'b	=	630.00 psi		F'v	=	139.50 psi	
Load Combination	=	D Only		Load Combination	=	D Only	
Location of maximum on span	=	6.941 ft		Location of maximum on span	=	13.412 ft	
Span # where maximum occurs	=	Span # 2		Span # where maximum occurs	=	Span # 2	
Maximum Deflection							
Max Downward Transient Deflection	0 in	Ratio =	0 < 360	n/a			
Max Upward Transient Deflection	0 in	Ratio =	0 < 360	n/a			
Max Downward Total Deflection	0.028 in	Ratio =	6097 >= 180	Span: 2 : D Only			
Max Upward Total Deflection	-0.009 in	Ratio =	3934 >= 180	Span: 1 : D Only			

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios										Moment Values			Shear Values		
Segment Length	Span #	M	V	CD	CM	C _t	CLx	C _F	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only																	
Length = 1.50 ft	1	0.003	0.011	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.01	1.7	630.0	0.04	1.5	139.5
Length = 14.0 ft	2	0.056	0.011	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.15	35.0	630.0	0.04	1.5	139.5
Length = 1.50 ft	3	0.003	0.011	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.01	1.7	630.0	0.01	1.5	139.5
+0.60D																	
Length = 1.50 ft	1	0.001	0.004	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.00	1.0	1,120.0	0.02	0.9	248.0
Length = 14.0 ft	2	0.019	0.004	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.09	21.0	1,120.0	0.02	0.9	248.0
Length = 1.50 ft	3	0.001	0.004	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.00	1.0	1,120.0	0.00	0.9	248.0

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Wood Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Roof Rafters

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.0000	0.000	D Only	-0.0091	0.000
	2	0.0276	7.059		0.0000	0.000
	3	0.0000	7.059	D Only	-0.0091	1.500

Vertical Reactions

Support notation : Far left is #1 Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4
Max Upward from all Load Conditions		0.055	0.055	
Max Upward from Load Combinations		0.033	0.033	
Max Upward from Load Cases		0.055	0.055	
D Only		0.055	0.055	
+0.60D		0.033	0.033	

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Roof Purlins

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : IBC 2021

Material Properties

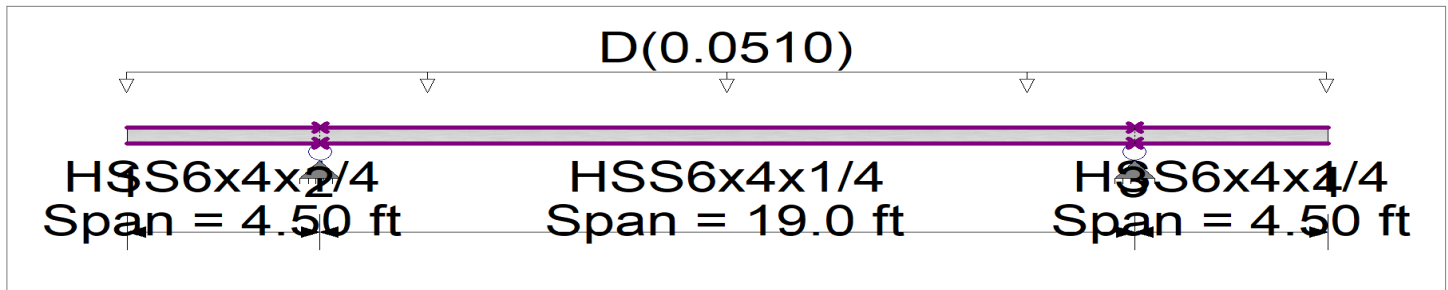
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

Loads on all spans...

Uniform Load on ALL spans : D = 0.0060 ksf, Tributary Width = 8.50 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.152 : 1	Maximum Shear Stress Ratio =		0.020 : 1
Section used for this span		HSS6x4x1/4	Section used for this span		HSS6x4x1/4
Ma : Applied		2.332 k-ft	Va : Applied		0.6329 k
Mn / Omega : Allowable		15.323 k-ft	Vn/Omega : Allowable		31.951 k
Load Combination		D Only	Load Combination		D Only
Span # where maximum occurs		Span # 2	Location of maximum on span		19.000 ft
Span # where maximum occurs		Span # 2	Span # where maximum occurs		Span # 2
Maximum Deflection					
Max Downward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Upward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Downward Total Deflection		0.238 in	Ratio =	959	>=180 Span: 3 : D Only
Max Upward Total Deflection		-0.152 in	Ratio =	709	>=180 Span: 3 : D Only

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values						Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega
D Only												
Dsgn. L = 4.50 ft	1	0.044	0.020		-0.67	0.67	25.59	15.32	1.00	1.00	0.63	53.36
Dsgn. L = 19.00 ft	2	0.152	0.020	2.33	-0.67	2.33	25.59	15.32	1.00	1.00	0.63	53.36
Dsgn. L = 4.50 ft	3	0.044	0.009		-0.67	0.67	25.59	15.32	1.00	1.00	0.30	53.36
+0.60D												
Dsgn. L = 4.50 ft	1	0.026	0.012		-0.40	0.40	25.59	15.32	1.00	1.00	0.38	53.36
Dsgn. L = 19.00 ft	2	0.091	0.012	1.40	-0.40	1.40	25.59	15.32	1.00	1.00	0.38	53.36
Dsgn. L = 4.50 ft	3	0.026	0.006		-0.40	0.40	25.59	15.32	1.00	1.00	0.18	53.36

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.0000	0.000	D Only	-0.1523	0.000
	2	0.2378	9.627	D Only	0.0000	0.000
	3	0.0000	9.627	D Only	-0.1524	4.500

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4
Max Upward from all Load Conditions		0.933	0.933	
Max Upward from Load Combinations		0.560	0.560	
Max Upward from Load Cases		0.933	0.933	
D Only		0.933	0.933	
+0.60D		0.560	0.560	

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: HSS A-Frame Beam Check

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : ASCE 7-16

Material Properties

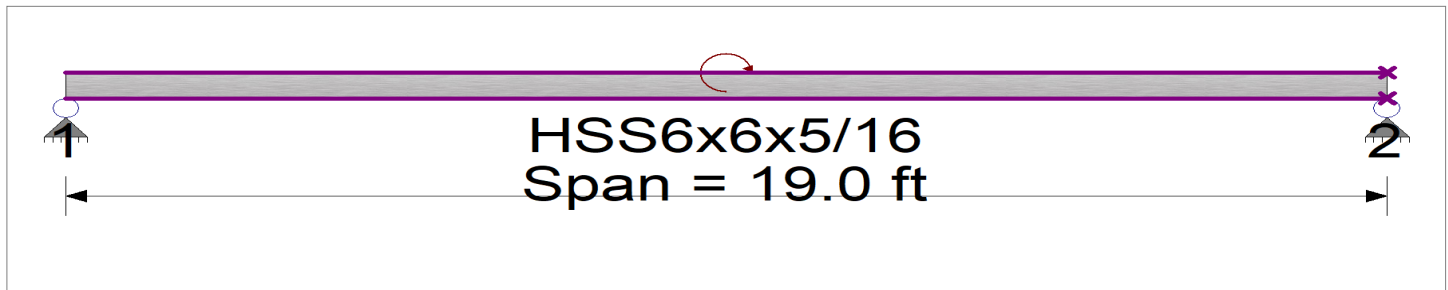
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight NOT internally calculated and added

Load(s) for Span Number 1

Moment : D = 5.161 k-ft, Loc = 9.50 ft in span, (Moment Check)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.106 : 1	Maximum Shear Stress Ratio =		0.007 : 1
Section used for this span		HSS6x6x5/16	Section used for this span		HSS6x6x5/16
Ma : Applied		2.581 k-ft	Va : Applied		0.2716 k
Mn / Omega : Allowable		24.431 k-ft	Vn/Omega : Allowable		38.594 k
Load Combination		D Only	Load Combination		D Only
Span # where maximum occurs		Span # 1	Location of maximum on span		0.000 ft
			Span # where maximum occurs		Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Upward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Downward Total Deflection		0.027 in	Ratio =	8525	>=180 Span: 1 : D Only
Max Upward Total Deflection		-0.026 in	Ratio =	8720	>=180 Span: 1 : D Only

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values						Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega
D Only												
Dsgn. L = 19.00 ft	1	0.106	0.007	2.57	-2.58	2.58	40.80	24.43	1.00	1.00	0.27	64.45 38.59
+0.60D												
Dsgn. L = 19.00 ft	1	0.063	0.004	1.54	-1.55	1.55	40.80	24.43	1.00	1.00	0.16	64.45 38.59

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.0267	13.626	D Only	-0.0261	5.537

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions		0.272 0.560
Max Upward from Load Combinations		0.163 0.560
Max Upward from Load Cases		0.272 0.560
Max Downward from all Load Conditions (Resi	-0.272	0.560
Max Downward from Load Combinations (Resi	-0.163	0.560
Max Downward from Load Cases (Resisting U	-0.272	0.560
D Only	-0.272	0.272 0.560
+0.60D	-0.163	0.163 0.560

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: HSS Deck Beam Check

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : ASCE 7-16

Material Properties

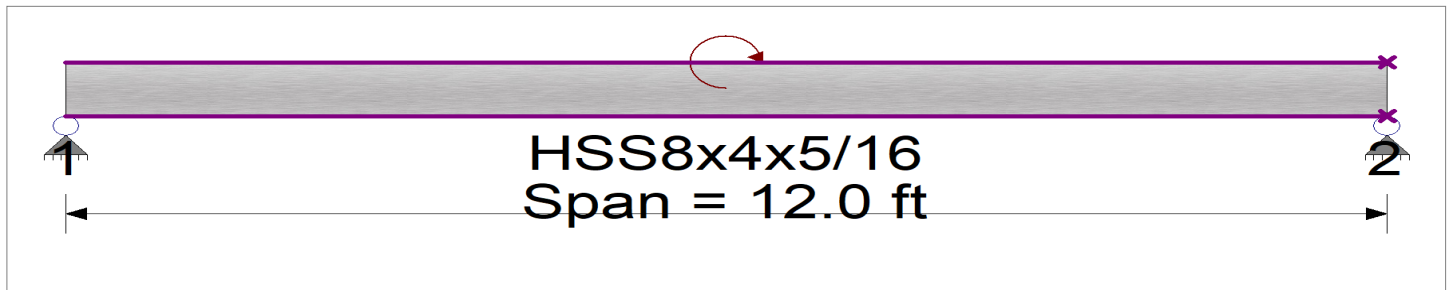
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight NOT internally calculated and added

Load(s) for Span Number 1

Moment : D = 2.484 k-ft, Loc = 6.0 ft in span, (Moment Check)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.043 : 1	Maximum Shear Stress Ratio =		0.004 : 1
Section used for this span		HSS8x4x5/16	Section used for this span		HSS8x4x5/16
Ma : Applied		1.242 k-ft	Va : Applied		0.2070 k
Mn / Omega : Allowable		28.922 k-ft	Vn/Omega : Allowable		53.650 k
Load Combination		D Only	Load Combination		D Only
Span # where maximum occurs		Span # 1	Location of maximum on span		0.000 ft
			Span # where maximum occurs		Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Upward Transient Deflection		0 in	Ratio =	0	<360 n/a
Max Downward Total Deflection		0.003 in	Ratio =	44985	>=180 Span: 1 : D Only
Max Upward Total Deflection		-0.003 in	Ratio =	42654	>=180 Span: 1 : D Only

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values							Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega	
D Only													
Dsgn. L = 12.00 ft	1	0.043	0.004	1.24	-1.23	1.24	48.30	28.92	1.00	1.00	0.21	89.59	53.65
+0.60D													
Dsgn. L = 12.00 ft	1	0.026	0.002	0.75	-0.74	0.75	48.30	28.92	1.00	1.00	0.12	89.59	53.65

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.0032	8.503	D Only	-0.0034	3.497

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions		0.207
Max Upward from Load Combinations		0.124
Max Upward from Load Cases		0.207
Max Downward from all Load Conditions (Resi)	-0.207	
Max Downward from Load Combinations (Resi)	-0.124	
Max Downward from Load Cases (Resisting U)	-0.207	
D Only	-0.207	0.207
+0.60D	-0.124	0.124

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Perpendicular Deck Beams

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : IBC 2021

Material Properties

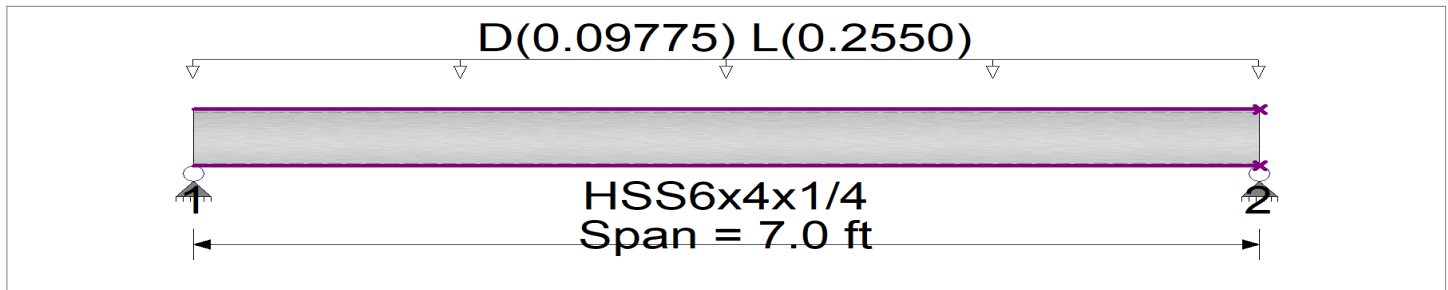
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

Uniform Load : D = 0.0230, L = 0.060 ksf, Tributary Width = 4.250 ft, (Uniform Deck Load)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.147 : 1	Maximum Shear Stress Ratio =		0.040 : 1
Section used for this span		HSS6x4x1/4	Section used for this span		HSS6x4x1/4
Ma : Applied		2.256 k-ft	Va : Applied		1.289 k
Mn / Omega : Allowable		15.323 k-ft	Vn/Omega : Allowable		31.951 k
Load Combination		+D+L	Load Combination		+D+L
Span # where maximum occurs		Span # 1	Location of maximum on span		0.000 ft
Span # where maximum occurs		Span # 1	Span # where maximum occurs		Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.023 in	Ratio =	3,678	>=360
Max Upward Transient Deflection		0 in	Ratio =	0	<360
Max Downward Total Deflection		0.033 in	Ratio =	2547	>=180
Max Upward Total Deflection		0 in	Ratio =	0	<180
					n/a

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values							Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
D Only													
Dsgn. L = 7.00 ft	1	0.045	0.012	0.69		0.69	25.59	15.32	1.00	1.00	0.40	53.36	31.95
+D+L													
Dsgn. L = 7.00 ft	1	0.147	0.040	2.26		2.26	25.59	15.32	1.00	1.00	1.29	53.36	31.95
+D+0.750L													
Dsgn. L = 7.00 ft	1	0.122	0.033	1.87		1.87	25.59	15.32	1.00	1.00	1.07	53.36	31.95
+0.60D													
Dsgn. L = 7.00 ft	1	0.027	0.007	0.42		0.42	25.59	15.32	1.00	1.00	0.24	53.36	31.95

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0330	3.520		0.0000	0.000

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.289	1.289
Max Upward from Load Combinations	1.289	1.289
Max Upward from Load Cases	0.893	0.893
Max Downward from all Load Conditions (Resi		0.560
Max Downward from Load Combinations (Resi		0.560
Max Downward from Load Cases (Resisting U		0.560
D Only	0.397	0.397
+D+L	1.289	1.289
+D+0.750L	1.066	1.066

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Perpendicular Deck Beams

Vertical Reactions		Support notation : Far left is #:		Values in KIPS
Load Combination	Support 1	Support 2		
+0.60D	0.238	0.238	0.560	
L Only	0.893	0.893	0.560	

Steel Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Steel Column Check

Code References

Calculations per AISC 360-16, IBC 2021, SDPWS 2021
Load Combinations Used : ASCE 7-16

General Information

Steel Section Name :	HSS6x6x5/16	Overall Column Height	10.0 ft
Analysis Method :	Allowable Strength	Top & Bottom Fixity	Top Free, Bottom Fixed
Steel Stress Grade		Brace condition :	
Fy : Steel Yield	36.0 ksi	Unbraced Length for buckling ABOUT X-X Axis =	10.0 ft, K = 2.1
E : Elastic Bending Modulus	29,000.0 ksi	Unbraced Length for buckling ABOUT Y-Y Axis =	10.0 ft, K = 2.1

Applied Loads

Service loads entered. Load Factors will be applied for calculations

Column self weight included : 233.40 lbs * Dead Load Factor
AXIAL LOADS . . .
Axial Load from Roof Purlin: Axial Load at 10.0 ft, D = 0.980 k
BENDING LOADS . . .
Seismic Load: Lat. Point Load at 10.0 ft creating Mx-x, E = 1.245 k

DESIGN SUMMARY

Bending & Shear Check Results

PASS Max. Axial+Bending Stress Ratio =	0.3649 : 1	Maximum Load Reactions . .	
Load Combination	+D+0.70E	Top along X-X	k
Location of max.above base	0.0 ft	Bottom along X-X	k
At maximum location values are . . .		Top along Y-Y	k
Pa : Axial	1.213 k	Bottom along Y-Y	k
Pn / Omega : Allowable	74.081 k	Maximum Load Deflections . . .	
Ma-x : Applied	-8.715 k-ft	Along Y-Y	in at ft above base
Mn-x / Omega : Allowable	24.431 k-ft	for load combination :	
Ma-y : Applied	0.0 k-ft	Along X-X	in at ft above base
Mn-y / Omega : Allowable	24.431 k-ft	for load combination :	
PASS Maximum Shear Stress Ratio	0.02258 : 1		
Load Combination	+D+0.70E		
Location of max.above base	0.0 ft		
At maximum location values are . . .			
Va : Applied	0.8715 k		
Vn / Omega : Allowable	38.594 k		

Load Combination Results

Load Combination	Maximum Axial + Bending Stress Ratios			Cb _x	Cb _y	K _x L _x /R _x	K _y L _y /R _y	Maximum Shear Ratios		
	Stress Ratio	Status	Location					Stress Ratio	Status	Location

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	Axial Reaction @ Base	X-X Axis Reaction @ Base @ Top	k	Y-Y Axis Reaction @ Base @ Top	Mx - End Moments @ Base @ Top	k-ft	My - End Moments @ Base @ Top
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Extreme Reactions

Item	Axial Reaction Extreme Value	X-X Axis Reaction @ Base @ Top	k	Y-Y Axis Reaction @ Base @ Top	Mx - End Moments @ Base @ Top	k-ft	My - End Moments @ Base @ Top
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Maximum Deflections for Load Combinations

Load Combination	Max. Deflection in X dir	Distance	Max. Deflection in Y dir	Distance
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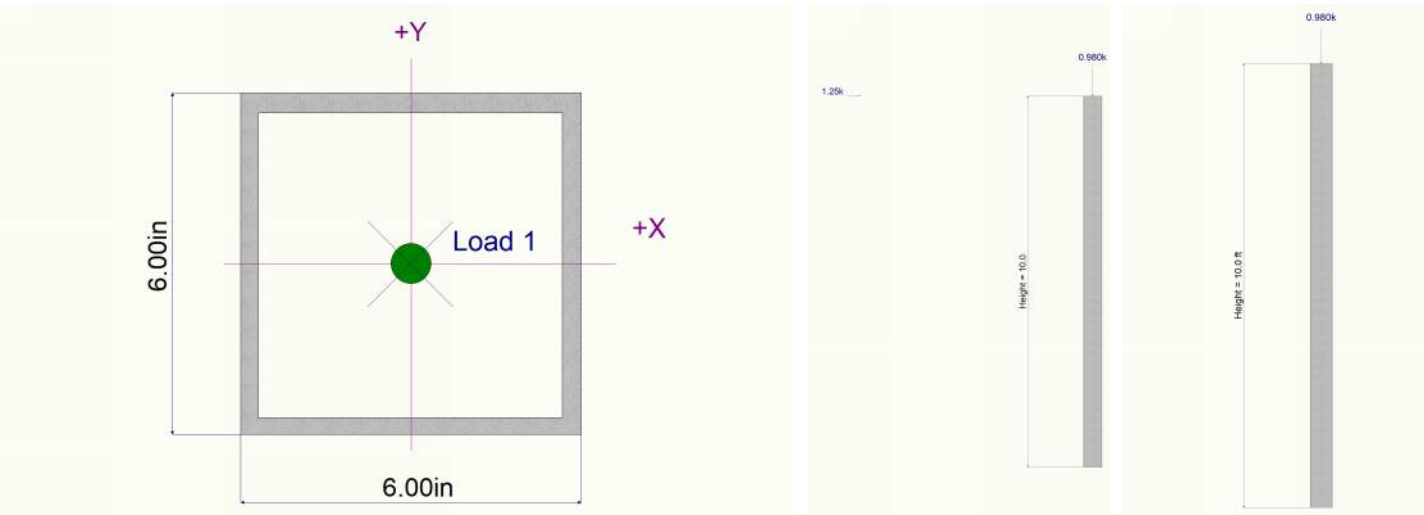
Steel Section Properties : HSS6x6x5/16

Steel Section Properties : HSS6x6x5/16

DESCRIPTION: Steel Column Check

Depth	=	6.000 in	I xx	=	34.30 in^4	J	=	55.400 in^4
Design Thick	=	0.291 in	S xx	=	11.40 in^3			
Width	=	6.000 in	R xx	=	2.310 in			
Wall Thick	=	0.313 in	Zx	=	13.600 in^3			
Area	=	6.430 in^2	I yy	=	34.300 in^4	C	=	18.900 in^3
Weight	=	23.340 plf	S yy	=	11.400 in^3			
			R yy	=	2.310 in			
Ycg	=	0.000 in						

Sketches



Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Parallel Deck Beams

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : IBC 2021

Material Properties

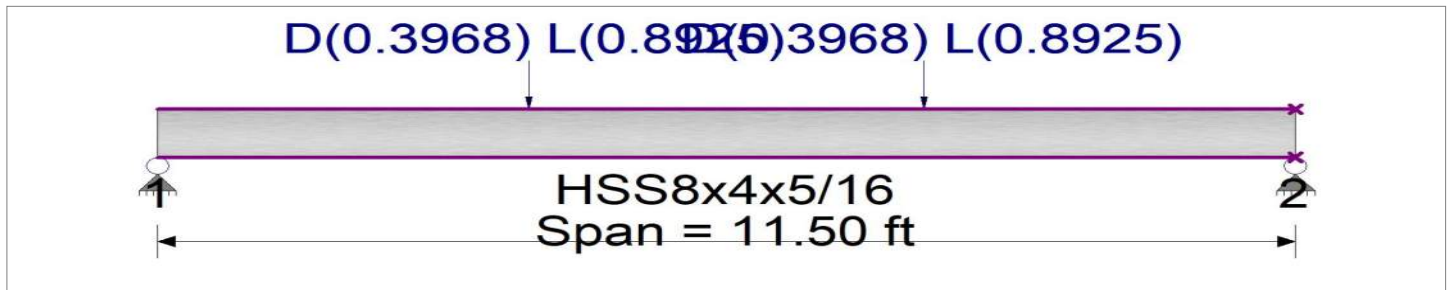
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

Linked Load(s)

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 3.75 ft from left end of beam

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 3.75 ft from left end of beam

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 7.75 ft from left end of beam

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 7.75 ft from left end of beam

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.348 : 1	Maximum Shear Stress Ratio =		0.051 : 1
Section used for this span		HSS8x4x5/16	Section used for this span		HSS8x4x5/16
Ma : Applied		10.056 k-ft	Va : Applied		2.713 k
Mn / Omega : Allowable		28.922 k-ft	Vn/Omega : Allowable		53.650 k
Load Combination		+D+L	Load Combination		+D+L
Span # where maximum occurs		Span # 1	Location of maximum on span		0.000 ft
Span # where maximum occurs		Span # 1	Span # where maximum occurs		Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.111 in Ratio = 1,238	>=360		Span: 1 : L Only
Max Upward Transient Deflection		0 in Ratio = 0	<360		n/a
Max Downward Total Deflection		0.167 in Ratio = 825	>=180		Span: 1 : +D+L
Max Upward Total Deflection		0 in Ratio = 0	<180		n/a

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values						Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega Cb	Rm	Va Max	Vnx	Vnx/Omega
D Only												
Dsgn. L = 11.50 ft	1	0.116	0.017	3.36		3.36	48.30	28.92 1.00 1.00		0.93	89.59	53.65
+D+L												
Dsgn. L = 11.50 ft	1	0.348	0.051	10.06		10.06	48.30	28.92 1.00 1.00		2.71	89.59	53.65
+D+0.750L												
Dsgn. L = 11.50 ft	1	0.290	0.042	8.38		8.38	48.30	28.92 1.00 1.00		2.27	89.59	53.65
+0.60D												
Dsgn. L = 11.50 ft	1	0.070	0.010	2.02		2.02	48.30	28.92 1.00 1.00		0.56	89.59	53.65

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1672	5.783		0.0000	0.000

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.713	2.713
Max Upward from Load Combinations	2.713	2.713
Max Upward from Load Cases	1.785	1.785
Max Downward from all Load Conditions (Resi)		0.560
Max Downward from Load Combinations (Resi)		0.560

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Parallel Deck Beams

Vertical Reactions		Support notation : Far left is #.		Values in KIPS
Load Combination	Support 1	Support 2		
Max Downward from Load Cases (Resisting U)				0.560
D Only	0.928	0.928		0.560
+D+L	2.713	2.713		0.560
+D+0.750L	2.267	2.267		0.560
+0.60D	0.557	0.557		0.560
L Only	1.785	1.785		0.560

Project Title: Lands of Wings Capital LLC
 Engineer: Daniel Byrne
 Project ID:
 Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Deck Rim Beam

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : IBC 2021

Material Properties

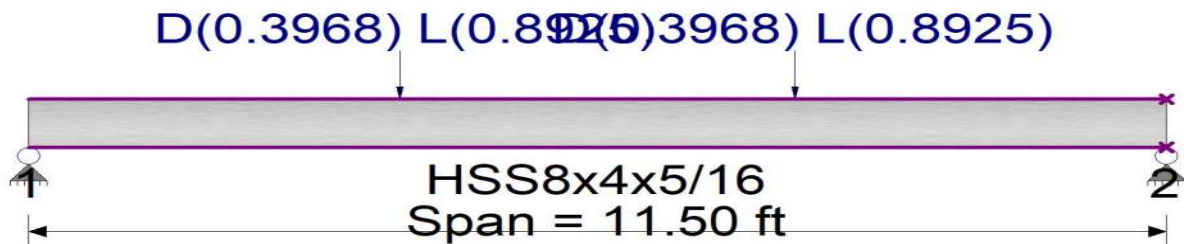
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

Linked Load(s)

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 3.75 ft from left end of beam

Beam Perpendicular Deck Beams, Support 1: D = 0.3968, L = 0.8925 k @ 7.75 ft from left end of beam

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.181 : 1		Maximum Shear Stress Ratio =		0.027 : 1	
Section used for this span		HSS8x4x5/16		Section used for this span		HSS8x4x5/16	
Ma : Applied		5.221 k-ft		Va : Applied		1.424 k	
Mn / Omega : Allowable		28.922 k-ft		Vn/Omega : Allowable		53.650 k	
Load Combination		+D+L		Load Combination		+D+L	
Span # where maximum occurs		Span # 1		Location of maximum on span		0.000 ft	
Span # where maximum occurs		Span # 1		Span # where maximum occurs		Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.056 in Ratio = 2,476		>=360		Span: 1 : L Only	
Max Upward Transient Deflection		0 in Ratio = 0		<360		n/a	
Max Downward Total Deflection		0.087 in Ratio = 1591		>=180		Span: 1 : +D+L	
Max Upward Total Deflection		0 in Ratio = 0		<180		n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values						Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega
D Only												
Dsgn. L = 11.50 ft	1	0.065	0.010	1.87		1.87	48.30	28.92	1.00	1.00	0.53	89.59
+D+L												
Dsgn. L = 11.50 ft	1	0.181	0.027	5.22		5.22	48.30	28.92	1.00	1.00	1.42	89.59
+D+0.750L												
Dsgn. L = 11.50 ft	1	0.152	0.022	4.38		4.38	48.30	28.92	1.00	1.00	1.20	89.59
+0.60D												
Dsgn. L = 11.50 ft	1	0.039	0.006	1.12		1.12	48.30	28.92	1.00	1.00	0.32	89.59

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0867	5.783		0.0000	0.000

Vertical Reactions

Support notation : Far left is #:

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.424	1.424
Max Upward from Load Combinations	1.424	1.424
Max Upward from Load Cases	0.893	0.893
Max Downward from all Load Conditions (Resi)		0.560
Max Downward from Load Combinations (Resi)		0.560
Max Downward from Load Cases (Resisting U)		0.560
D Only	0.531	0.531

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Deck Rim Beam

Vertical Reactions

Support notation : Far left is #. Values in KIPS

Load Combination	Support 1	Support 2	
+D+L	1.424	1.424	0.560
+D+0.750L	1.200	1.200	0.560
+0.60D	0.319	0.319	0.560
L Only	0.893	0.893	0.560

Project Title: Lands of Wings Capital LLC
 Engineer: Daniel Byrne
 Project ID:
 Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC#: KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Deck Beams along Lines 1 & 2

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, SDPWS 2021

Load Combination Set : ASCE 7-16

Material Properties

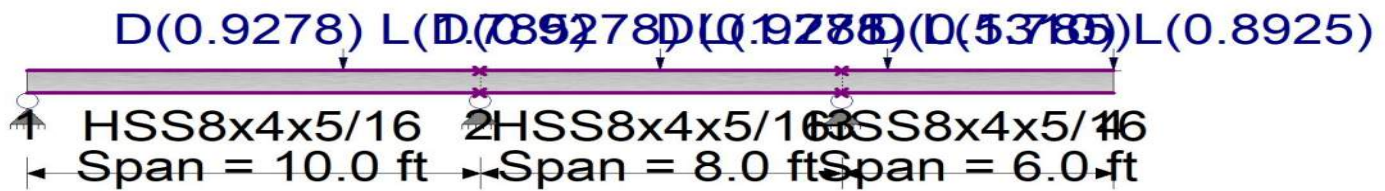
Analysis Method Allowable Strength Design

Fy : Steel Yield : 36.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Beam self weight calculated and added to loading

Linked Load(s)

Beam Deck Rim Beam, Support 1: D = 0.5310, L = 0.8925 k @ 24 ft from left end of beam

Beam Parallel Deck Beams, Support 1: D = 0.9278, L = 1.785 k @ 7 ft from left end of beam

Beam Parallel Deck Beams, Support 1: D = 0.9278, L = 1.785 k @ 14 ft from left end of beam

Beam Parallel Deck Beams, Support 1: D = 0.9278, L = 1.785 k @ 19 ft from left end of beam

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =		0.404 : 1	Maximum Shear Stress Ratio =		0.080 : 1
Section used for this span		HSS8x4x5/16	Section used for this span		HSS8x4x5/16
Ma : Applied		11.674 k-ft	Va : Applied		4.276 k
Mn / Omega : Allowable		28.922 k-ft	Vn/Omega : Allowable		53.650 k
Load Combination		+D+L	Load Combination		+D+L
Span # where maximum occurs		Span # 2	Location of maximum on span		8.000 ft
Span # where maximum occurs		Span # 2	Span # where maximum occurs		Span # 2
Maximum Deflection					
Max Downward Transient Deflection		0.177 in Ratio = 814 >=360	Span: 3 : L Only		
Max Upward Transient Deflection		-0.019 in Ratio = 4,972 >=360	Span: 3 : L Only		
Max Downward Total Deflection		0.291 in Ratio = 494 >=180	Span: 3 : +D+L		
Max Upward Total Deflection		-0.032 in Ratio = 2985 >=180	Span: 3 : +D+L		

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stress Ratios		Summary of Moment Values						Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega
D Only												
Dsgn. L = 10.00 ft	1	0.057	0.016	1.65	-0.78	1.65	48.30	28.92	1.00	1.00	0.84	89.59
Dsgn. L = 8.00 ft	2	0.157	0.030	-0.00	-4.53	4.53	48.30	28.92	1.00	1.00	1.60	89.59
Dsgn. L = 6.00 ft	3	0.157	0.030		-4.53	4.53	48.30	28.92	1.00	1.00	1.60	89.59
+D+L												
Dsgn. L = 10.00 ft	1	0.153	0.042	4.44	-2.15	4.44	48.30	28.92	1.00	1.00	2.23	89.59
Dsgn. L = 8.00 ft	2	0.404	0.080	-0.00	-11.67	11.67	48.30	28.92	1.00	1.00	4.28	89.59
Dsgn. L = 6.00 ft	3	0.404	0.080		-11.67	11.67	48.30	28.92	1.00	1.00	4.28	89.59
+D+0.750L												
Dsgn. L = 10.00 ft	1	0.129	0.035	3.74	-1.81	3.74	48.30	28.92	1.00	1.00	1.88	89.59
Dsgn. L = 8.00 ft	2	0.342	0.067	-0.00	-9.89	9.89	48.30	28.92	1.00	1.00	3.61	89.59
Dsgn. L = 6.00 ft	3	0.342	0.067		-9.89	9.89	48.30	28.92	1.00	1.00	3.61	89.59
+0.60D												
Dsgn. L = 10.00 ft	1	0.034	0.009	0.99	-0.47	0.99	48.30	28.92	1.00	1.00	0.51	89.59
Dsgn. L = 8.00 ft	2	0.094	0.018	-0.00	-2.72	2.72	48.30	28.92	1.00	1.00	0.96	89.59
Dsgn. L = 6.00 ft	3	0.094	0.018		-2.72	2.72	48.30	28.92	1.00	1.00	0.96	89.59

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0408	5.400		0.0000	0.000

Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Steel Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Deck Beams along Lines 1 & 2

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
	2	0.0000	5.400	+D+L	-0.0322	5.173
+D+L	3	0.2913	6.000		0.0000	5.173

Vertical Reactions

Support notation : Far left is #: Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4
Max Upward from all Load Conditions	0.716	2.490	6.917	
Max Upward from Load Combinations	0.716	2.490	6.917	
Max Upward from Load Cases	0.398	1.559	4.291	
D Only	0.317	0.931	2.626	
+D+L	0.716	2.490	6.917	
+D+0.750L	0.616	2.100	5.844	
+0.60D	0.190	0.559	1.575	
L Only	0.398	1.559	4.291	



T R U N O R T H

FOUNDATION CALCULATIONS



TRUNORTH

PIER DESIGN (A-FRAME BASE)

Minimum pier diameter per Geotech = 12"

Pier diameter used = 18"

Skin friction = 500 psf

Circumference of pier = 4.712 ft

Allowable downward dead + live load per foot
of embedment = $500 \times 4.712 = 2356 \text{ plf}$

With a safety factor of 1.5 = 1570.7 plf

Allowable uplift frictional capacity = $2/3 \times 1570.7$
= 1047.1 plf

Max. uplift from attached calculations = 4401 lbs

Minimum pier embedment required = $\frac{4401}{1047.1}$
= 4.2 ft

Ignoring top 3 ft of weak soils,
embedment required = 8 ft

⇒ Downward capacity provided = 1570.7×5
= 7853.5 lbs

DEAD LOAD $\approx 40 \text{ PSF}$
LIVE LOAD $\approx 60 \text{ PSF}$

125 SF WUorst case = $5000 + 7500 \text{ L} = 12.5 \text{ K}$

$12,500 / 1570.7 = 7.96$, use 8' + 3'
= 11' MIN



T R U N O R T H

PIER DESIGN (STEPS).

Pier diameter used = 18"

Circumference of pier = 4.712 ft

Skin friction = 500 psf

Allowable downward dead + live load per
foot of embedment = 500×4.712
= 2356 plf

With a safety factor of 1.5 = 1570.7 plf.

Max. downward load from attached
grade beam calculations = 32464 lbs.

Provide total 3 piers along grade beam.



T R U N O R T H

$$\begin{aligned}\text{Max. downward load on each pier} &= \frac{32464}{3} \\ &= 10821.3 \text{ lbs.}\end{aligned}$$

$$\begin{aligned}\text{Minimum embedment required} &= \frac{10821.3}{1570.7} \\ &= 6.89 \text{ ft}\end{aligned}$$

Ignoring top 3ft of weak soils,
total embedment required = 10 ft

Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Code References

Calculations per ACI 318-19, IBC 2021, SDPWS 2021
Load Combinations Used : ASCE 7-16

General Information

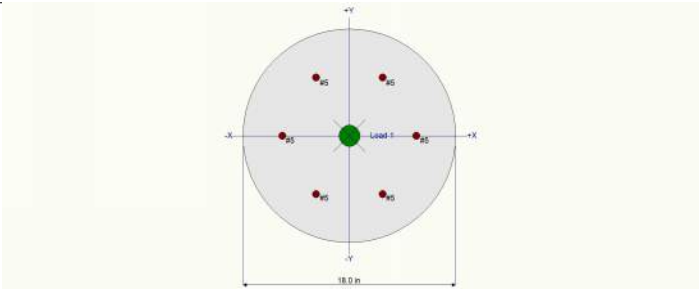
f'_c : Concrete 28 day strength	=	2.50 ksi
E =	=	3122 ksi
Density	=	150 pcf
β	=	0.850
f_y - Main Rebar	=	60 ksi
E - Main Rebar	=	29000 ksi
Allow. Reinforcing Limits	ASTM A615 Bars Used	
Min. Reinf.	=	0.50 %
Max. Reinf.	=	8 %
Seismic Design Category	=	A

Overall Column Height	=	6.0 ft
End Fixity	Top Free, Bottom Fixed	
Brace condition for deflection (buckling) along colour		
X-X (width) axis :		
Unbraced Length for buckling ABOUT X-X Axis = 6.0 ft, K = 0.80		
Y-Y (depth) axis :		
Unbraced Length for buckling ABOUT Y-Y Axis = 6.0 ft, K = 0.80		

Column Cross Section

Column Dimensions : 18.0in Diameter, Column Edge to Rebar Edge Cover = 3.0in

Column Reinforcing : 6 - #5 bars



Applied Loads

Entered loads are factored per load combinations specified by user

Column self weight included : 1,590.43 lbs * Dead Load Factor
AXIAL LOADS . . .
Axial Loads at each pier: Axial Load at 6.0 ft above base, D = 3.50 k
BENDING LOADS . . .
Lateral Load at each pier: Lat. Point Load at 6.0 ft creating Mx-x, E = 3.50 k

DESIGN SUMMARY

Load Combination	+0.90D+E	Maximum SERVICE Load Reactions .			
Location of max.above base	5.960 ft	Top along Y-Y	0.0 k	Bottom along Y-Y	0.0 k
Maximum Stress Ratio		Top along X-X	0.0 k	Bottom along X-X	3.50 k
Ratio = $(P_u^2 + M_u^2)^{.5} / (\phi P_n^2 + \phi M_n^2)^{.5}$		Maximum SERVICE Load Deflections . .			
P_u =	4.581 k	$\phi * P_n$ =	13.653 k	Along Y-Y	0.02693 in at 6.0 ft above base
M_{u-x} =	-21.0 k-ft	$\phi * M_{n-x}$ =	58.838 k-ft	for load combination : E Only	
M_{u-y} =	0.4352 k-ft	$\phi * M_{n-y}$ =	0.8757 k-ft	Along X-X	0.0 in at 0.0 ft above base
M_u Angle =	1.0 deg	ϕ =	0.90	for load combination :	
M_u at Angle =	21.005 k-ft	ϕM_n at Angle =	58.241 k-ft	General Section Information	
P_n & M_n values located at P_u - M_u vector intersection with capacity curve				β = 0.850	θ = 0.850
Column Capacities . .		ρ : % Reinforcing	0.7309 %	Rebar % Ok	
P_{nmax} : Nominal Max. Compressive Axial Capac	648.39 k	Reinforcing Area	1.860 in ²	Concrete Area	254.469 in ²
P_{nmin} : Nominal Min. Tension Axial Capacity	k				
ϕP_n , max : Usable Compressive Axial Capacity	413.351 k				
ϕP_n , min : Usable Tension Axial Capacity	k				

Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03 TruNorth (c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Governing Load Combination Results

Governing Factored Load Combination	Moment		Dist. from base ft	Axial Load k		Bending Analysis k-ft						Utilization	
	X-X	Y-Y		Pu	$\phi * Pn$	δx	$\delta x * Mux$	δy	$\delta y * Muy$	Alpha (deg)	δMu	ϕ Mn	Ratio
+1.40D	Actual	M2,min	5.96	7.13	407.33	1.000		1.000	0.68	90.000	0.68	38.40	0.018
+1.40D	M2,min	Actual	5.96	7.13	407.26	1.000	0.68	1.000		0.000	0.68	38.09	0.018
+1.20D	Actual	M2,min	5.96	6.11	407.33	1.000		1.000	0.58	90.000	0.58	38.40	0.015
+1.20D	M2,min	Actual	5.96	6.11	407.26	1.000	0.58	1.000		0.000	0.58	38.09	0.015
+0.90D	Actual	M2,min	5.96	4.58	407.33	1.000		1.000	0.44	90.000	0.44	38.40	0.011
+0.90D	M2,min	Actual	5.96	4.58	407.26	1.000	0.44	1.000		0.000	0.44	38.09	0.011
+1.20D+E	Actual	M2,min	5.96	6.11	16.46	1.000	-21.00	1.000	0.58	2.000	21.01	59.43	0.354
+0.90D+E	Actual	M2,min	5.96	4.58	13.65	1.000	-21.00	1.000	0.44	1.000	21.00	58.24	0.361

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction @ Base	Mx - End Moments k-ft		My - End Moments k-ft	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
D Only						5.090				
+0.60D						3.054				
+D+0.70E				2.450		5.090	-14.700			
+D+0.5250E				1.838		5.090	-11.025			
+0.60D+0.70E				2.450		3.054	-14.700			
E Only				3.500			-21.000			

Maximum Moment Reactions

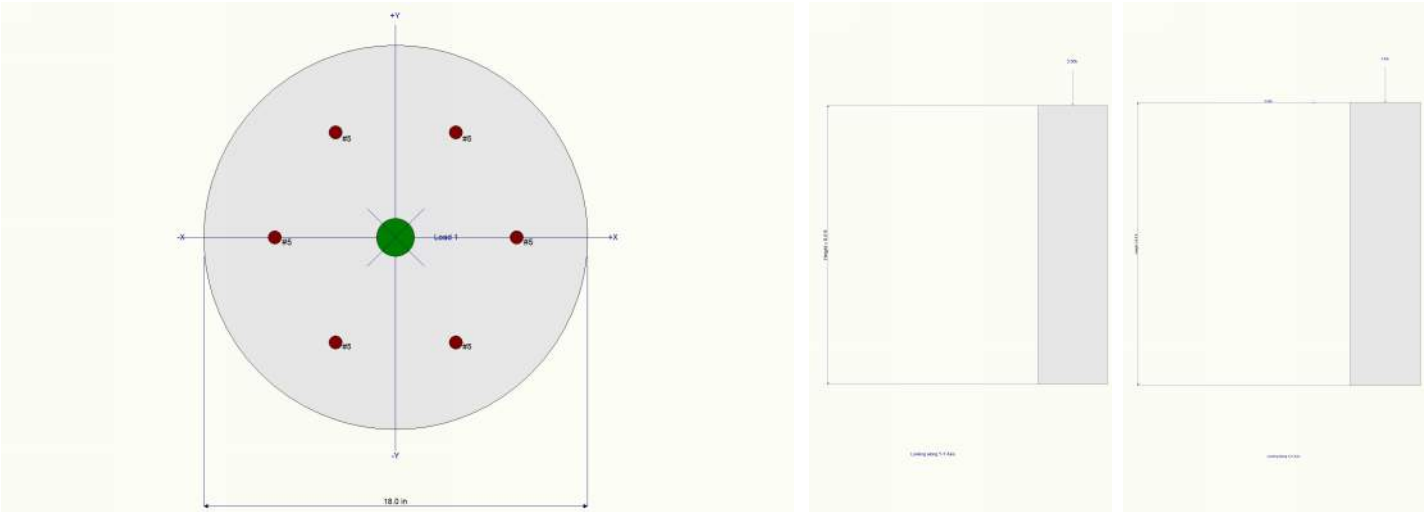
Note: Only non-zero reactions are listed.

Load Combination	Moment About X-X Axis		k-ft	Moment About Y-Y Axis		k-ft
	@ Base	@ Top		@ Base	@ Top	
D Only						
+0.60D						
+D+0.70E	-14.700					
+D+0.5250E	-11.025					
+0.60D+0.70E	-14.700					
E Only	-21.000					

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000 ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000 ft	0.000 in	0.000 ft
+D+0.70E	0.0000 in	0.000 ft	0.019 in	6.000 ft
+D+0.5250E	0.0000 in	0.000 ft	0.014 in	6.000 ft
+0.60D+0.70E	0.0000 in	0.000 ft	0.019 in	6.000 ft
E Only	0.0000 in	0.000 ft	0.027 in	5.960 ft

Sketches



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

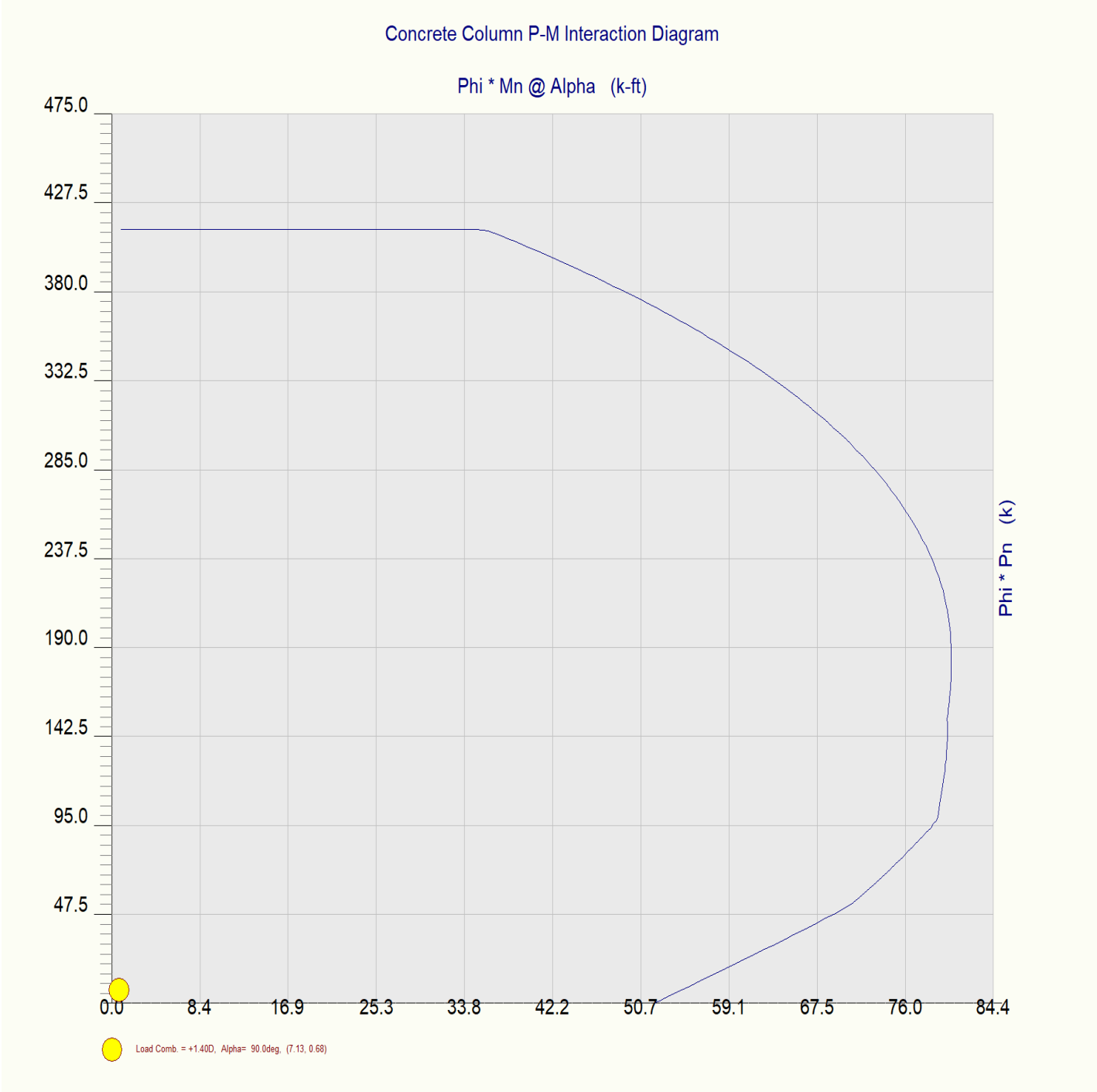
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Interaction Diagrams



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

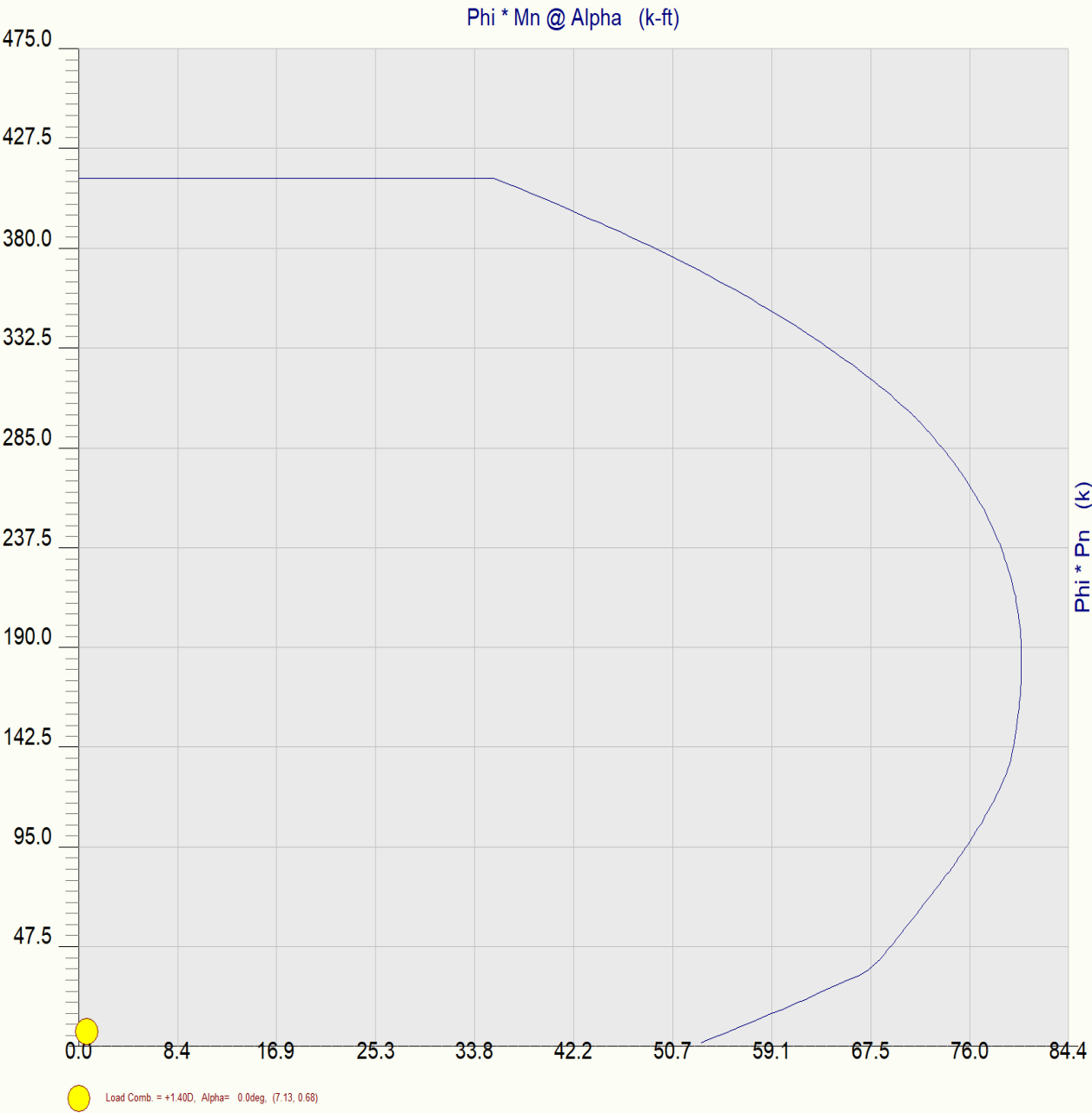
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

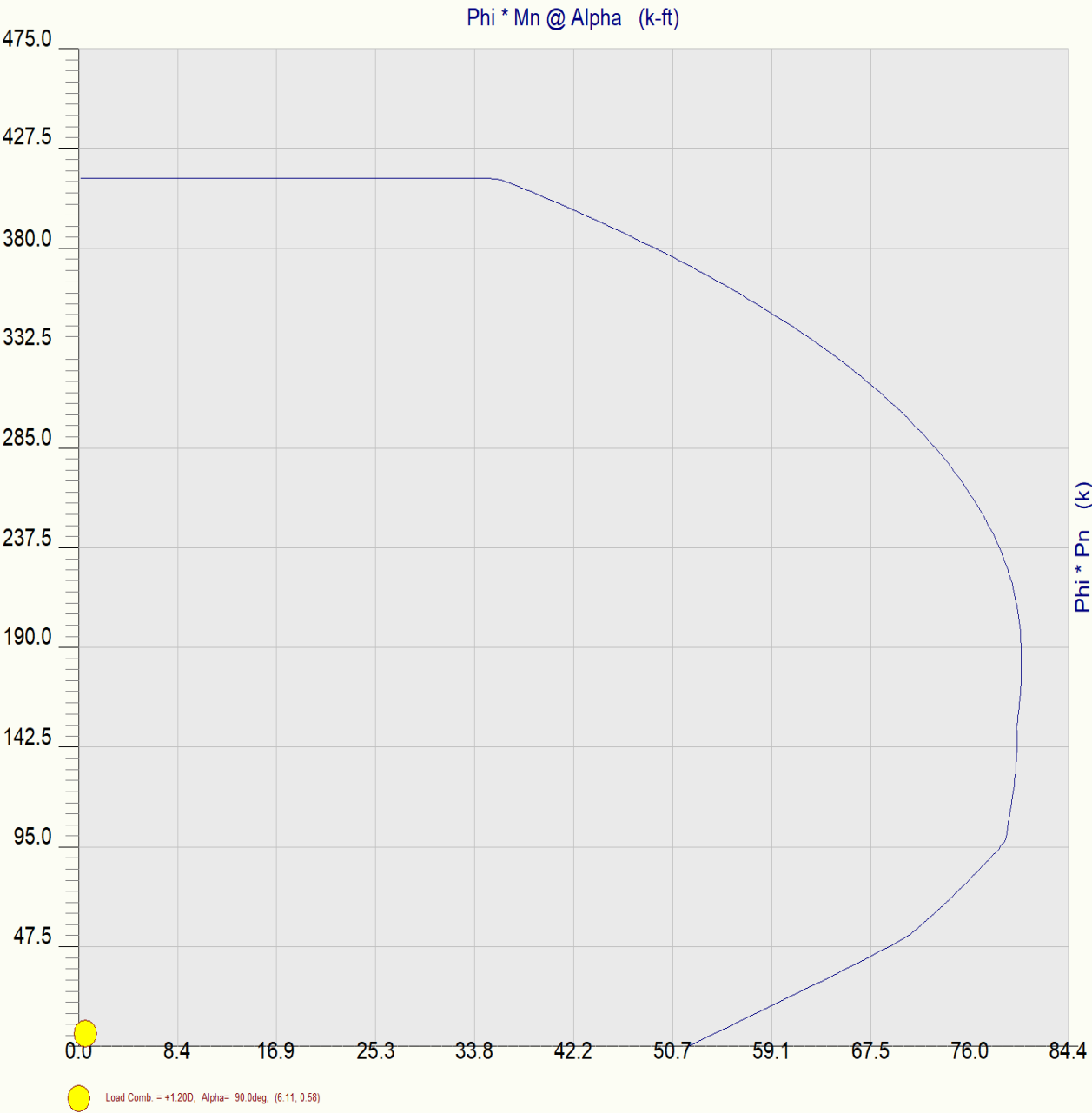
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

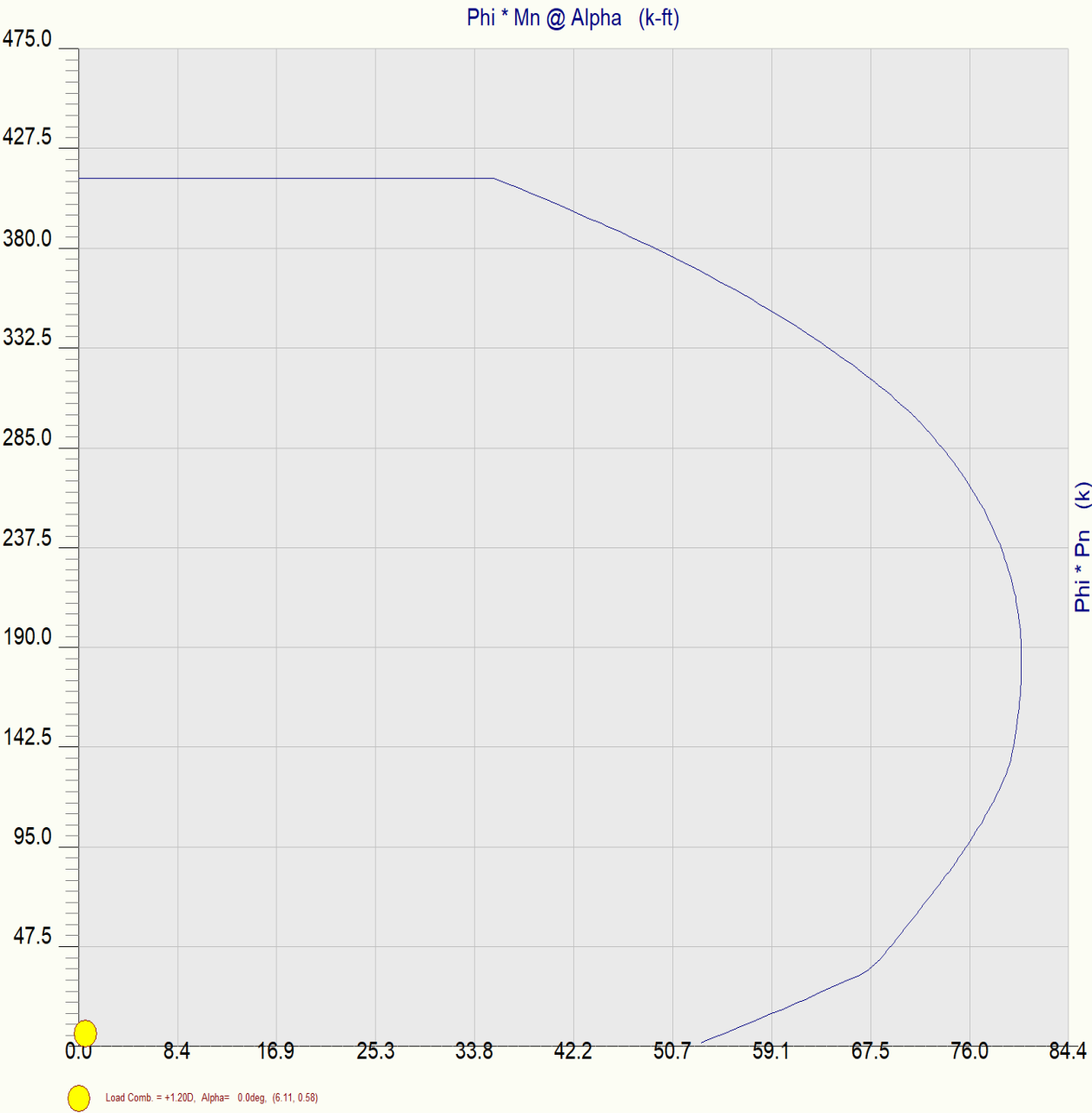
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

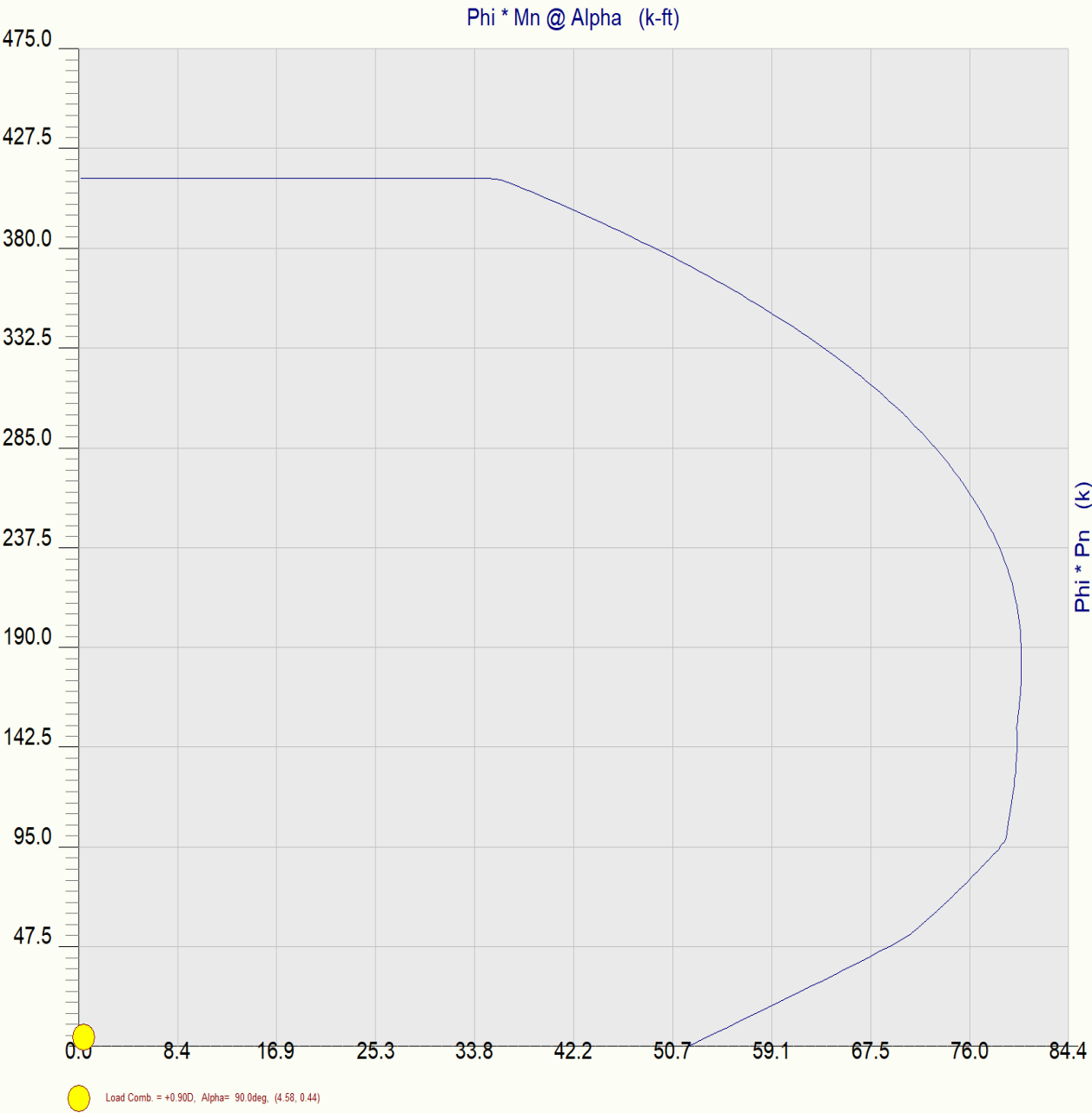
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

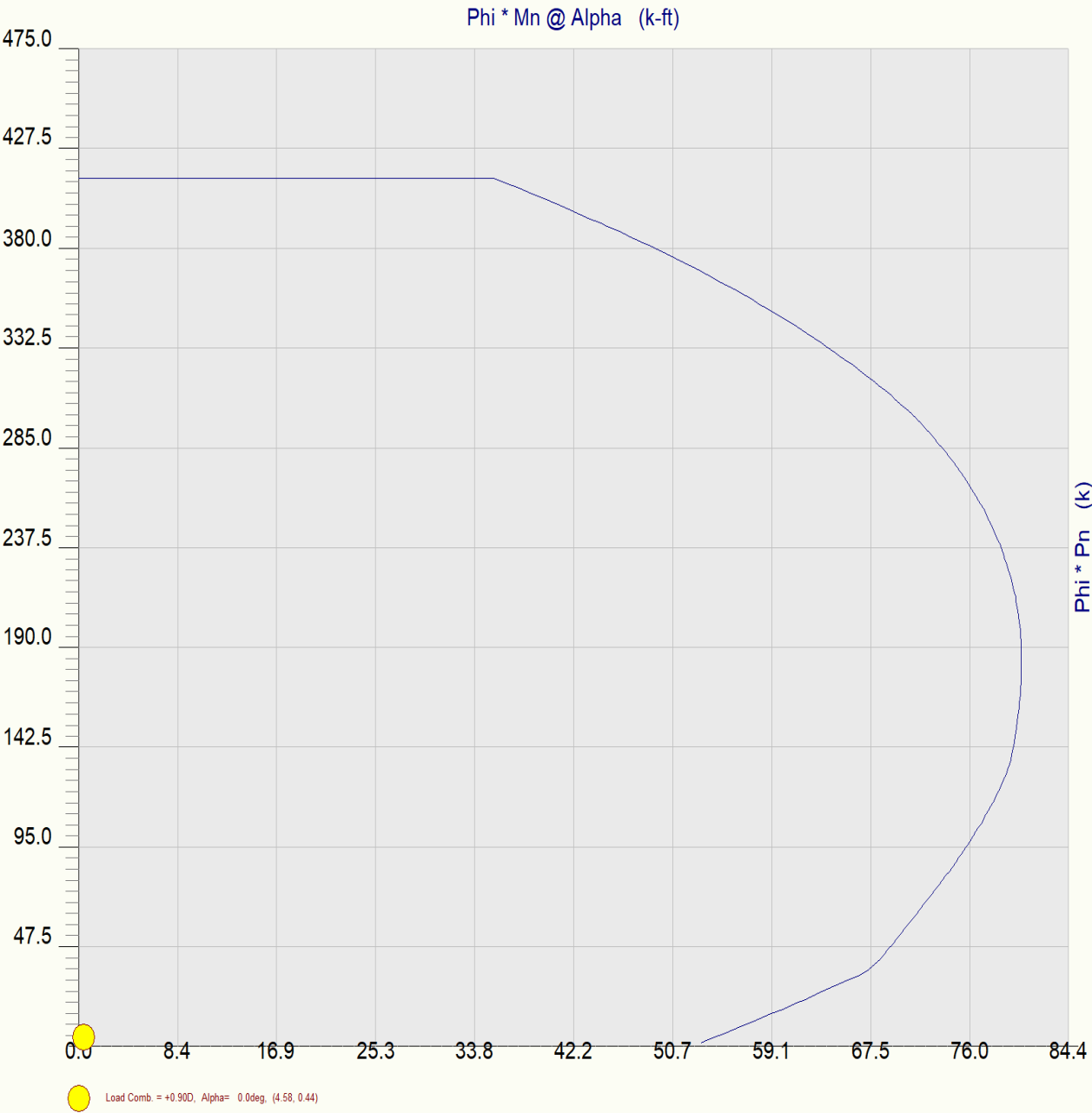
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

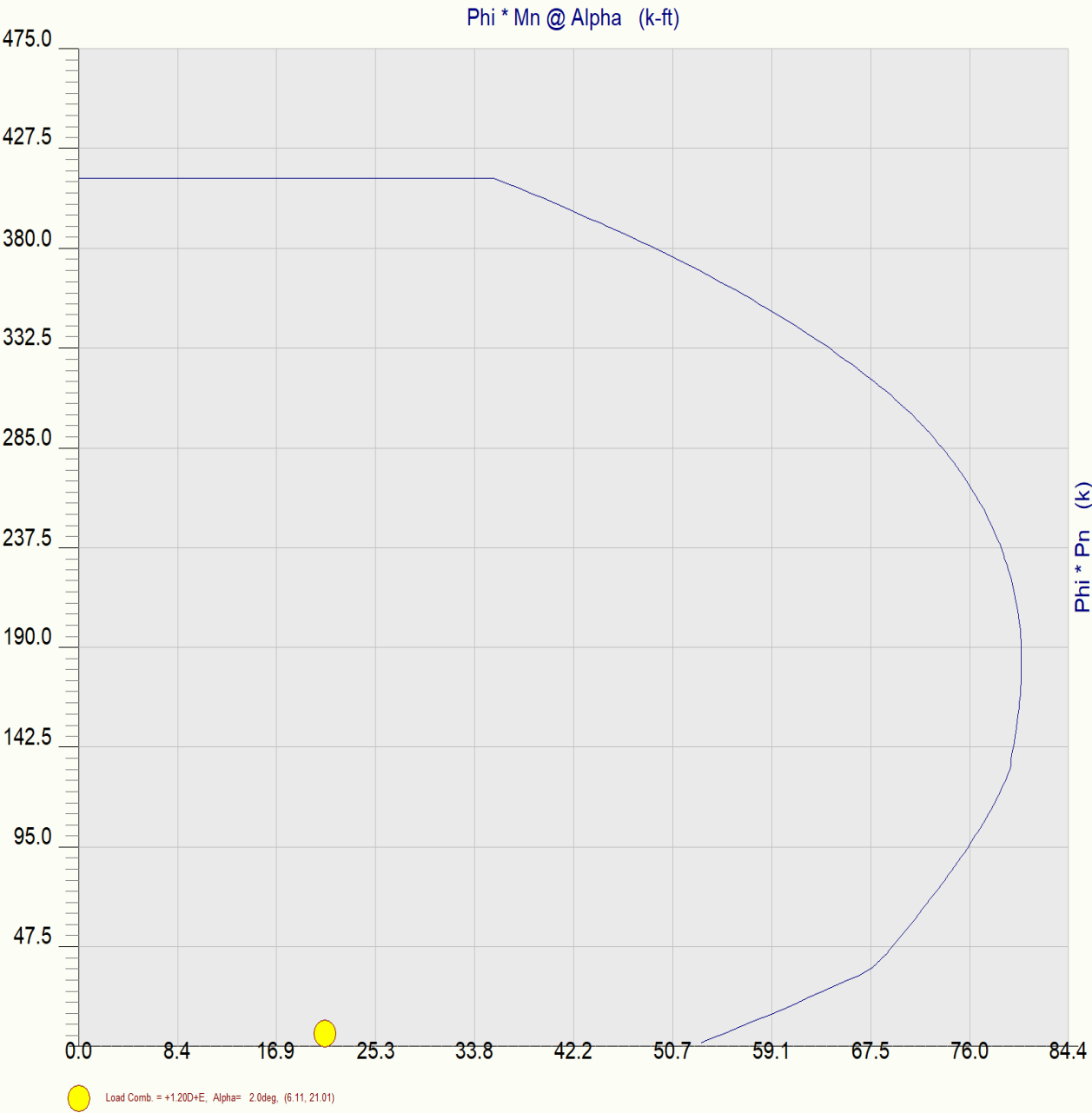
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Concrete Column

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

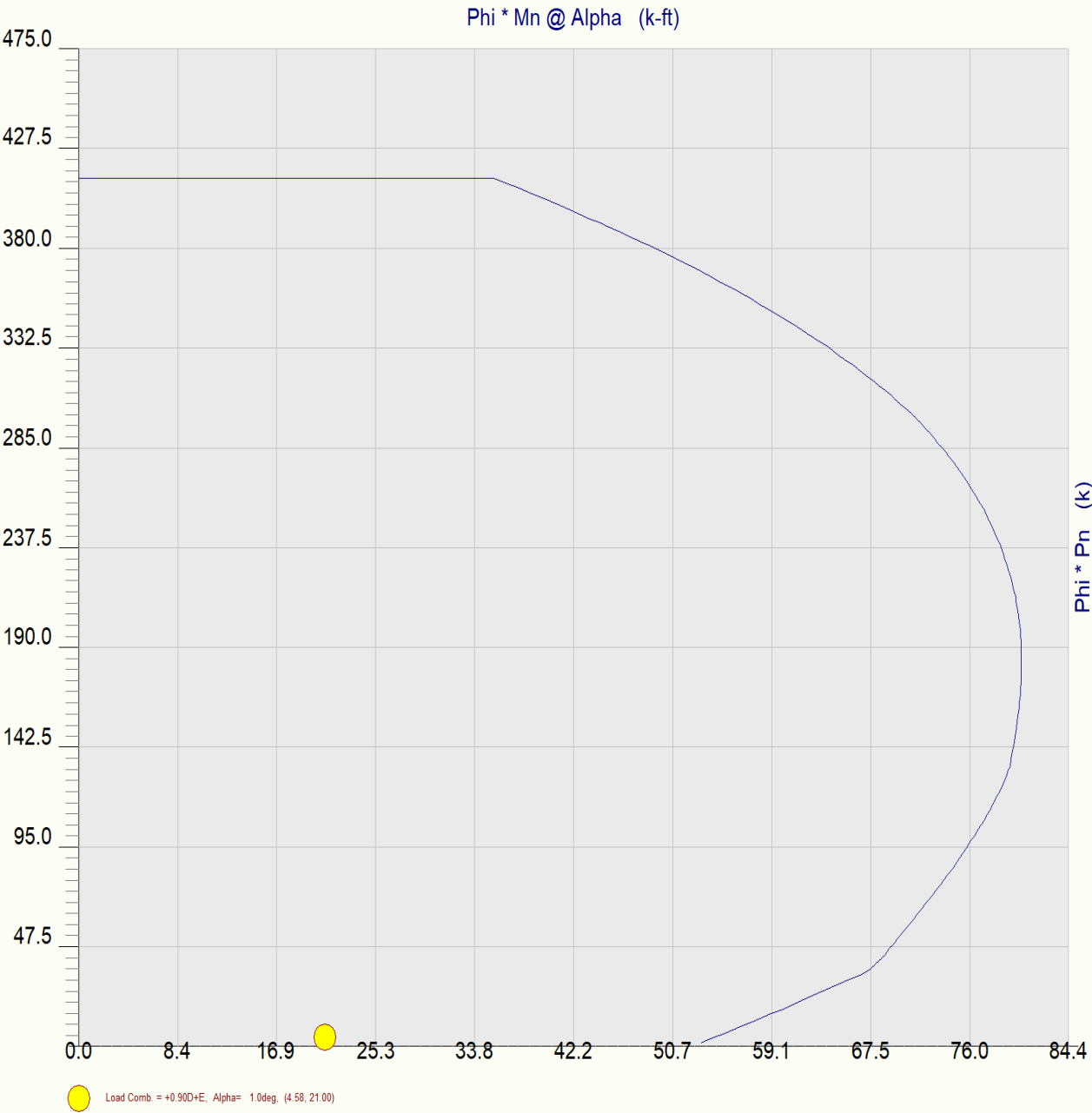
LIC# : KW-06020862, Build:20.24.09.03

TruNorth

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DESCRIPTION: Piers at A-Frame Columns

Concrete Column P-M Interaction Diagram



Project Title: Lands of Wings Capital LLC
Engineer: Daniel Byrne
Project ID:
Project Descr: New Deck

Concrete Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

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DESCRIPTION: Grade Beam at Steps

CODE REFERENCES

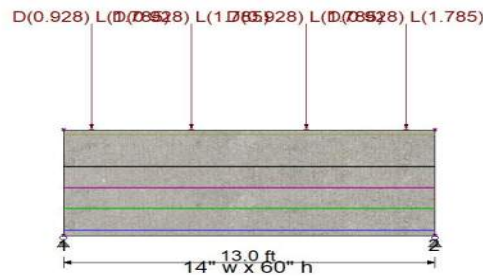
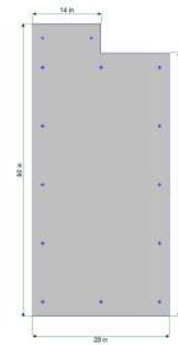
Calculations per ACI 318-19, IBC 2021, SDPWS 2021

Load Combination Set : ASCE 7-16

General Information

f'_c	=	2.50 ksi	ϕ Phi Values	Flexure :	0.90
$f_r = f'_c^{1/2} \cdot 7.50$	=	375.0 psi		Shear :	0.750
ψ Density	=	150.0 pcf	β_1	=	0.850
λ LtWt Factor	=	1.0			
Elastic Modulus	=	3,122.0 ksi	Fy - Stirrups	=	40.0 ksi
f_y - Main Rebar	=	60.0 ksi	E - Stirrups	=	29,000.0 ksi
E - Main Rebar	=	29,000.0 ksi	Stirrup Bar Size #	=	3
			Number of Resisting Legs Per Stirrup	=	2

Seismic Design Category = A



Cross Section & Reinforcing Details

L Section, Stem Width = 14.0 in, Total Height = 60.0 in, Bottom Flange Width = 28.0 in, Flange Thickness = 54.0 in

Span #1 Reinforcing....

3-#5 at 3.0 in from Bottom, from 0.0 to 13.0 ft in this span	2-#5 at 15.0 in from Bottom, from 0.0 to 13.0 ft in this span
2-#5 at 27.0 in from Bottom, from 0.0 to 13.0 ft in this span	2-#5 at 21.0 in from Top, from 0.0 to 13.0 ft in this span
3-#5 at 9.0 in from Top, from 0.0 to 13.0 ft in this span	2-#4 at 3.0 in from Top, from 0.0 to 13.0 ft in this span

Beam self weight calculated and added to loads

Point Load : D = 0.9280, L = 1.785 k @ 1.0 ft, (Load from Deck Beam)
Point Load : D = 0.9280, L = 1.785 k @ 4.50 ft, (Load from Deck Beam)
Point Load : D = 0.9280, L = 1.785 k @ 8.50 ft, (Load from Deck Beam)
Point Load : D = 0.9280, L = 1.785 k @ 12.0 ft, (Load from Deck Beam)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =	0.131 : 1
Section used for this span	Typical Section
Mu : Applied	63.977 k-ft
Mn * Phi : Allowable	489.467 k-ft
Location of maximum on span	6.488 ft
Span # where maximum occurs	Span # 1

Maximum Deflection

Max Downward Transient Deflection	0.000 in	Ratio =	0 <360.0	L Only
Max Upward Transient Deflection	0.000 in	Ratio =	0 <360.0	L Only
Max Downward Total Deflection	0.001 in	Ratio =	138874 >=180.0	Span: 1 : +D+L
Max Upward Total Deflection	0.000 in	Ratio =	0 <180.0	Span: 1 : +D+L

Vertical Reactions

Support notation : Far left is #1

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	16.232	16.232
Max Upward from Load Combinations	16.232	16.232

Project Title: Lands of Wings Capital LLC
 Engineer: Daniel Byrne
 Project ID:
 Project Descr: New Deck

Concrete Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Grade Beam at Steps

Vertical Reactions

Support notation : Far left is #1

Load Combination	Support 1	Support 2
Max Upward from Load Cases	12.662	12.662
D Only	12.662	12.662
+D+L	16.232	16.232
+D+0.750L	15.340	15.340
+0.60D	7.597	7.597
L Only	3.570	3.570

Shear Stirrup Requirements

Between 0.00 to 0.99 ft, Max spacing per T9.7.6.2.2, use #3 stirrups spaced at 23 in

Between 1.02 to 11.98 ft, Ties Not Req'd, Stirrups are not required.

Between 12.01 to 12.98 ft, Max spacing per T9.7.6.2.2, use #3 stirrups spaced at 23 in

Detailed Shear Information

Load Combination	Span Number	Distance (ft)	'd' (in)	Vu (k)	Av, min Req'd?	Spacing Req'd (in)	ϕ Vc (k)	ϕ Vs (k)	ϕ Vn (k)	Vu / ϕ Vn	Vc Eqn (T22.5.5.1)	Spacing Provision
+1.20D+1.60L	1	0.00	46.71	20.91	No	23.36	15.53	13.20	28.73	0.728	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.14	46.71	20.62	No	23.36	15.53	13.20	28.73	0.718	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.28	46.71	20.34	No	23.36	15.53	13.20	28.73	0.708	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.43	46.71	20.06	No	23.36	15.53	13.20	28.73	0.698	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.57	46.71	19.77	No	23.36	15.53	13.20	28.73	0.688	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.71	46.71	19.49	No	23.36	15.53	13.20	28.73	0.678	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.85	46.71	19.21	No	23.36	15.53	13.20	28.73	0.668	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	0.99	46.71	18.92	No	23.36	15.53	13.20	28.73	0.659	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	1.14	46.71	14.67	No	N/A	15.53	0.00	15.53	0.944	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.28	46.71	14.39	No	N/A	15.53	0.00	15.53	0.926	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.42	46.71	14.10	No	N/A	15.53	0.00	15.53	0.908	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.56	46.71	13.82	No	N/A	15.53	0.00	15.53	0.890	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.70	46.71	13.54	No	N/A	15.53	0.00	15.53	0.871	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.85	46.71	13.25	No	N/A	15.53	0.00	15.53	0.853	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	1.99	46.71	12.97	No	N/A	15.53	0.00	15.53	0.835	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.13	46.71	12.69	No	N/A	15.53	0.00	15.53	0.817	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.27	46.71	12.40	No	N/A	15.53	0.00	15.53	0.798	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.42	46.71	12.12	No	N/A	15.53	0.00	15.53	0.780	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.56	46.71	11.84	No	N/A	15.53	0.00	15.53	0.762	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.70	46.71	11.55	No	N/A	15.53	0.00	15.53	0.744	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.84	46.71	11.27	No	N/A	15.53	0.00	15.53	0.725	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	2.98	46.71	10.98	No	N/A	15.53	0.00	15.53	0.707	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.13	46.71	10.70	No	N/A	15.53	0.00	15.53	0.689	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.27	46.71	10.42	No	N/A	15.53	0.00	15.53	0.671	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.41	46.71	10.13	No	N/A	15.53	0.00	15.53	0.652	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.55	46.71	9.85	No	N/A	15.53	0.00	15.53	0.634	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.69	46.71	9.57	No	N/A	15.53	0.00	15.53	0.616	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.84	46.71	9.28	No	N/A	15.53	0.00	15.53	0.598	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	3.98	46.71	9.00	No	N/A	15.53	0.00	15.53	0.579	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	4.12	46.71	8.72	No	N/A	15.53	0.00	15.53	0.561	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	4.26	46.71	8.43	No	N/A	15.53	0.00	15.53	0.543	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	4.40	46.71	8.15	No	N/A	15.53	0.00	15.53	0.525	Eqn (c)	Ties Not Req'd
+1.40D	1	4.55	46.71	4.55	No	N/A	15.53	0.00	15.53	0.293	Eqn (c)	Ties Not Req'd
+1.40D	1	4.69	46.71	4.22	No	N/A	15.53	0.00	15.53	0.271	Eqn (c)	Ties Not Req'd
+1.40D	1	4.83	46.71	3.89	No	N/A	15.53	0.00	15.53	0.250	Eqn (c)	Ties Not Req'd
+1.40D	1	4.97	46.71	3.55	No	N/A	15.53	0.00	15.53	0.229	Eqn (c)	Ties Not Req'd
+1.40D	1	5.11	46.71	3.22	No	N/A	15.53	0.00	15.53	0.208	Eqn (c)	Ties Not Req'd
+1.40D	1	5.26	46.71	2.89	No	N/A	15.53	0.00	15.53	0.186	Eqn (c)	Ties Not Req'd
+1.40D	1	5.40	46.71	2.56	No	N/A	15.53	0.00	15.53	0.165	Eqn (c)	Ties Not Req'd
+1.40D	1	5.54	46.71	2.23	No	N/A	15.53	0.00	15.53	0.144	Eqn (c)	Ties Not Req'd
+1.40D	1	5.68	46.71	1.90	No	N/A	15.53	0.00	15.53	0.122	Eqn (c)	Ties Not Req'd
+1.40D	1	5.83	46.71	1.57	No	N/A	15.53	0.00	15.53	0.101	Eqn (c)	Ties Not Req'd
+1.40D	1	5.97	46.71	1.24	No	N/A	15.53	0.00	15.53	0.080	Eqn (c)	Ties Not Req'd
+1.40D	1	6.11	46.71	0.91	No	N/A	15.53	0.00	15.53	0.059	Eqn (c)	Ties Not Req'd
+1.40D	1	6.25	46.71	0.58	No	N/A	15.53	0.00	15.53	0.037	Eqn (c)	Ties Not Req'd
+1.40D	1	6.39	46.71	0.25	No	N/A	15.53	0.00	15.53	0.016	Eqn (c)	Ties Not Req'd
+1.40D	1	6.54	46.71	-0.08	No	N/A	15.53	0.00	15.53	0.005	Eqn (c)	Ties Not Req'd
+1.40D	1	6.68	46.71	-0.41	No	N/A	15.53	0.00	15.53	0.027	Eqn (c)	Ties Not Req'd
+1.40D	1	6.82	46.71	-0.74	No	N/A	15.53	0.00	15.53	0.048	Eqn (c)	Ties Not Req'd
+1.40D	1	6.96	46.71	-1.07	No	N/A	15.53	0.00	15.53	0.069	Eqn (c)	Ties Not Req'd
+1.40D	1	7.10	46.71	-1.41	No	N/A	15.53	0.00	15.53	0.090	Eqn (c)	Ties Not Req'd
+1.40D	1	7.25	46.71	-1.74	No	N/A	15.53	0.00	15.53	0.112	Eqn (c)	Ties Not Req'd
+1.40D	1	7.39	46.71	-2.07	No	N/A	15.53	0.00	15.53	0.133	Eqn (c)	Ties Not Req'd

Project Title: Lands of Wings Capital LLC
 Engineer: Daniel Byrne
 Project ID:
 Project Descr: New Deck

Concrete Beam

Project File: 2199 Diamond Mountain Rd Deck Calculations.ec6

LIC# : KW-06020862, Build:20.24.09.03

TruNorth

(c) ENERCALC, LLC 1982-2024

DESCRIPTION: Grade Beam at Steps

Detailed Shear Information

Load Combination	Span Number	Distance (ft)	'd' (in)	Vu (k)	Av, min Req'd?	Spacing Req'd (in)	ϕV_c (k)	ϕV_s (k)	ϕV_n (k)	Vu / ϕV_n	Vc Eqn (T22.5.5.1)	Spacing Provision
+1.40D	1	7.53	46.71	-2.40	No	N/A	15.53	0.00	15.53	0.154	Eqn (c)	Ties Not Req'd
+1.40D	1	7.67	46.71	-2.73	No	N/A	15.53	0.00	15.53	0.176	Eqn (c)	Ties Not Req'd
+1.40D	1	7.81	46.71	-3.06	No	N/A	15.53	0.00	15.53	0.197	Eqn (c)	Ties Not Req'd
+1.40D	1	7.96	46.71	-3.39	No	N/A	15.53	0.00	15.53	0.218	Eqn (c)	Ties Not Req'd
+1.40D	1	8.10	46.71	-3.72	No	N/A	15.53	0.00	15.53	0.239	Eqn (c)	Ties Not Req'd
+1.40D	1	8.24	46.71	-4.05	No	N/A	15.53	0.00	15.53	0.261	Eqn (c)	Ties Not Req'd
+1.40D	1	8.38	46.71	-4.38	No	N/A	15.53	0.00	15.53	0.282	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	8.52	46.71	-8.01	No	N/A	15.53	0.00	15.53	0.516	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	8.67	46.71	-8.29	No	N/A	15.53	0.00	15.53	0.534	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	8.81	46.71	-8.58	No	N/A	15.53	0.00	15.53	0.552	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	8.95	46.71	-8.86	No	N/A	15.53	0.00	15.53	0.570	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.09	46.71	-9.14	No	N/A	15.53	0.00	15.53	0.589	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.23	46.71	-9.43	No	N/A	15.53	0.00	15.53	0.607	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.38	46.71	-9.71	No	N/A	15.53	0.00	15.53	0.625	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.52	46.71	-9.99	No	N/A	15.53	0.00	15.53	0.643	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.66	46.71	-10.28	No	N/A	15.53	0.00	15.53	0.662	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.80	46.71	-10.56	No	N/A	15.53	0.00	15.53	0.680	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	9.95	46.71	-10.84	No	N/A	15.53	0.00	15.53	0.698	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.09	46.71	-11.13	No	N/A	15.53	0.00	15.53	0.716	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.23	46.71	-11.41	No	N/A	15.53	0.00	15.53	0.735	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.37	46.71	-11.69	No	N/A	15.53	0.00	15.53	0.753	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.51	46.71	-11.98	No	N/A	15.53	0.00	15.53	0.771	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.66	46.71	-12.26	No	N/A	15.53	0.00	15.53	0.789	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.80	46.71	-12.54	No	N/A	15.53	0.00	15.53	0.807	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	10.94	46.71	-12.83	No	N/A	15.53	0.00	15.53	0.826	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.08	46.71	-13.11	No	N/A	15.53	0.00	15.53	0.844	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.22	46.71	-13.39	No	N/A	15.53	0.00	15.53	0.862	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.37	46.71	-13.68	No	N/A	15.53	0.00	15.53	0.880	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.51	46.71	-13.96	No	N/A	15.53	0.00	15.53	0.899	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.65	46.71	-14.24	No	N/A	15.53	0.00	15.53	0.917	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.79	46.71	-14.53	No	N/A	15.53	0.00	15.53	0.935	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	11.93	46.71	-14.81	No	N/A	15.53	0.00	15.53	0.953	Eqn (c)	Ties Not Req'd
+1.20D+1.60L	1	12.08	46.71	-19.06	No	23.36	15.53	13.20	28.73	0.663	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.22	46.71	-19.35	No	23.36	15.53	13.20	28.73	0.673	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.36	46.71	-19.63	No	23.36	15.53	13.20	28.73	0.683	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.50	46.71	-19.91	No	23.36	15.53	13.20	28.73	0.693	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.64	46.71	-20.20	No	23.36	15.53	13.20	28.73	0.703	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.79	46.71	-20.48	No	23.36	15.53	13.20	28.73	0.713	Eqn (c)	Max spacing per T9.7.6.
+1.20D+1.60L	1	12.93	46.71	-20.76	No	23.36	15.53	13.20	28.73	0.723	Eqn (c)	Max spacing per T9.7.6.

Maximum Forces & Stresses for Load Combinations

Load Combination	Span #	Location (ft) along Beam	Bending Stress Results (k-ft)		
Segment			Mu : Max	Phi*Mnx	Stress Ratio
MAXimum BENDING Envelope					
Span # 1	1	13.000	63.98	489.47	0.13
+1.40D					
Span # 1	1	13.000	56.31	489.47	0.12
+1.20D+1.60L					
Span # 1	1	13.000	63.98	489.47	0.13
+1.20D+L					
Span # 1	1	13.000	58.09	489.47	0.12
+1.20D					
Span # 1	1	13.000	48.27	489.47	0.10
+0.90D					
Span # 1	1	13.000	36.20	489.47	0.07

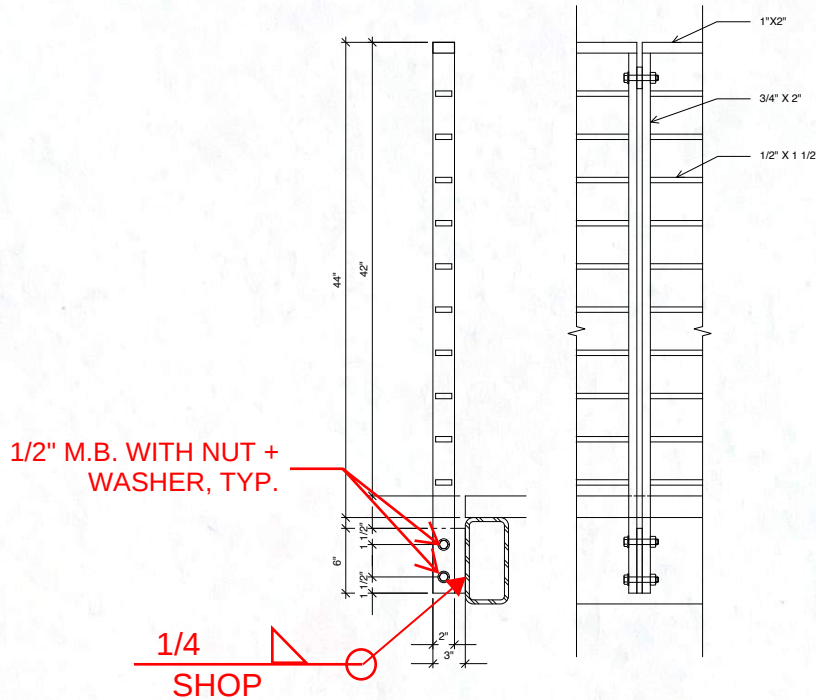
Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl (in)	Location in Span (ft)	Load Combination	Max. "+" Defl (in)	Location in Span (ft)
+D+L	1	0.0011	6.500		0.0000	0.000



TRUNORTH

GUARD RAIL CONNECTION



$$M_u = 44" \times 200 \text{ lbs} = 8800 \text{ lbs.}$$

$$M_u < \frac{M_n}{\Omega} \quad (\text{ASD}).$$

$$\Omega = 1.67 \quad (\text{AISC F.1})$$

$$M_n > 1.67 \times 8800 = 14696 \text{ in. lbs.}$$

$$M_p = Z_x \cdot F_y$$

$$Z_x = \frac{bh^2}{6} = \frac{2 \times 1.5^2}{6} = 0.75 \text{ in}^3$$

$$F_y = 36,000 \text{ psi} \quad (\text{A36 steel}).$$

$$M_p = 0.75 \times 36000 = 27,000 \text{ in. lbs.}$$



T R U N O R T H

$$\begin{aligned}\text{Reaction at bolt connection} &= \frac{14696}{3} \\ &= 4898.67 \text{ kips.}\end{aligned}$$

$$\begin{aligned}\text{Nominal shear strength of } 1/2" \text{ bolts} &= F_{nv} A_b \\ &= 54000 \text{ psi (A325 bolts)} \times \frac{\pi}{4} \times 0.5^2 \quad \text{(AISC J3-1) } F_{nv} A_b \\ &= 10,602.9 \text{ kips.} \quad \text{J3-1) } 0.5^2\end{aligned}$$

$$\begin{aligned}\text{Strength of weld} &= 14.85 \text{ kips/in.} \\ 14.85 \times (114") \times l &> 14696 \text{ in. kips.}\end{aligned}$$

$$l > \frac{14696}{14.85 \times 0.25} = 3.96 \text{ in.}$$

Total weld length provided is 6" each side,
12" total. de,
12" total.